

## 带有 I<sup>2</sup>C 兼容接口和遥感的 4A 处理器电源

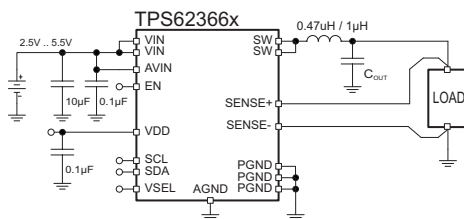
 查询样品: [TPS62366A](#), [TPS62366B](#)

### 特性

- **4A** 峰值输出电流
- 最高效率:
  - 低  $R_{DS}$ , 接通开关和有源整流器
  - 用于轻负载的省电模式
- **I<sup>2</sup>C** 高速兼容接口
- 用于数字电压调节的可编程输出电压
  - **0.5V 至 1.77V**, 步长 **10mV**
- 出色的 **DC/AC** 输出电压调节
  - 差分负载感测
  - 精准的 **DC** 输出电压精度
  - **DCS-Control™** 用于快速和精确瞬态调节的架构
- 多重稳健的操作/保护功能:
  - 软启动
  - 电压转换时的可编程转换率
  - 过热保护
  - 内部电压检测/闭锁
- 采用 **16 凸块, 2mm x 2mm NanoFree™** 封装
- 低外部器件数量 **< 25mm<sup>2</sup>** 解决方案尺寸

### 应用范围

- 应用处理器和数字信号处理器 (**DSP**) 电源
- 动态电压调节 **SmartReflex™** 兼容处理器电源
- 手机、智能手机、功能手机
- 平板电脑、掌上电脑 (**PDA**), 移动互联网设备 (**MID**), 上网本



### 说明

TPS62366x 是一款高频同步降压 dc/dc 转换器, 此转换器针对小型解决方案尺寸内的电池供电类便携式应用进行了优化。借助于 2.5V 至 5.5V 的输入电压范围, 此器件支持通用电池技术。此器件提供 4A 峰值负载电流, 运行在 2.5MHz 典型开关频率上。

此器件转换至一个 0.5V 至 1.77V 的输出电压范围内, 并可通过 I<sup>2</sup>C 接口以 10mV 为步长进行编程。专用输入可实现快速电压转换来寻址处理器性能工作点。

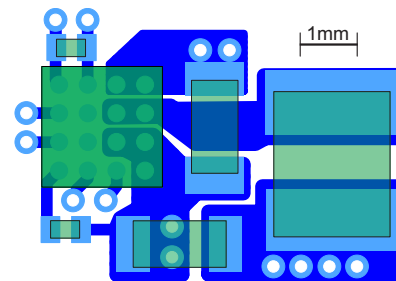
TPS62366x 支持低压 DSP 和智能手机以及包括最新亚微米工艺的手持计算机中的处理器内核。一个专用硬件输入引脚允许到性能工作点和处理器保持模式的简单转换。

此器件专注于高输出电压精度。此差分感测和 DCS-Control™ 架构可实现精准静态和动态、瞬态输出电压调节。

TPS62366x 器件提供高效降压转换。最高效的领域被扩展至低输出电流以使处理器运行在保持模式的同时提高效率, 此领域也被扩展至最高输出电流来延长电池接通时间。

稳健的架构和多重安全特性可实现理想的系统集成。

所采用的 2mm x 2mm 封装和少量外部组件量实现了小于 25mm<sup>2</sup> 的极小型解决方案尺寸。



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

DCS-Control, NanoFree, SmartReflex are trademarks of Texas Instruments.



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

**ORDERING INFORMATION**

PART NUMBER	PACKAGE MARKING	PACKAGE	DEVICE SPECIFIC FEATURES <sup>(1)</sup>	
			Output Voltage Range	Output Voltage Presets
TPS62366A <sup>(2)</sup>	See <a href="#">PACKAGE SUMMARY</a> Section	CSP-16	V <sub>OUT</sub> = 0.5V to 1.77V, 10mV Steps	1.20V, 1.16V
TPS62366B <sup>(3)</sup>	See <a href="#">PACKAGE SUMMARY</a> Section	CSP-16	V <sub>OUT</sub> = 0.5V to 1.77V, 10mV Steps	0.96V, 1.40V

- (1) Contact the factory to check availability of other output voltage or feature versions.
- (2) The YZH package is available in tape and reel. Add R suffix (TPS62366AYZHR) to order quantities of 3000 parts per reel, T suffix for 250 parts per reel (TPS62366AYZHT). For the most current package and ordering information, see the Package Option Addendum at the end of this document, or visit the device product folder on ti.com.
- (3) The YZH package is available in tape and reel. Add R suffix (TPS62366BYZHR) to order quantities of 3000 parts per reel, T suffix for 250 parts per reel (TPS62366BYZHT). For the most current package and ordering information, see the Package Option Addendum at the end of this document, or visit the device product folder on ti.com.

**ABSOLUTE MAXIMUM RATINGS**

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		VALUE		UNIT
		MIN	MAX	
Voltage range <sup>(2)</sup>	VIN, AVIN, SW pin	-0.3	7	V
	EN, VSEL, SENSE+	-0.3	(V <sub>AVIN</sub> +0.3V)	V
	SENSE-	-0.3	0.3	V
	SCL, SDA	-0.3	(V <sub>DD</sub> +0.3V)	V
	VDD	-0.3	3.6	V
Continuous RMS VIN / SW current per Pin <sup>(3)</sup>	T <sub>A</sub> < 85°C		1275	mA
Temperature range	Operating junction temperature, T <sub>J</sub>	-40	150	°C
	Storage temperature, T <sub>stg</sub>	-65	150	°C
ESD rating <sup>(4)</sup>	Machine model		200	V
	Charge device model		500	V
	Human body model		2	kV

- (1) Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) All voltage values are with respect to network ground terminal.
- (3) In order to be consistent with the TI reliability requirement for the silicon chips (100K Power-On-Hours at 105°C junction temperature), the current should not continuously exceed 2550mA in the VIN pins and 2550mA in the SW pins so as to prevent electromigration failure in the solder. See [THERMAL AND DEVICE LIFETIME INFORMATION](#).
- (4) The human body model is a 100-pF capacitor discharged through a 1.5-kΩ resistor into each pin. The machine model is a 200-pF capacitor discharged directly into each pin.

**THERMAL INFORMATION**

THERMAL METRIC <sup>(1)</sup>		TPS62366x		UNITS
		YZH		
		16 PINS		
$\theta_{JA}$	Junction-to-ambient thermal resistance <sup>(2)</sup>	94.8		°C/W
$\theta_{JCTop}$	Junction-to-case (top) thermal resistance <sup>(3)</sup>	25		
$\theta_{JB}$	Junction-to-board thermal resistance <sup>(4)</sup>	60		
$\psi_{JT}$	Junction-to-top characterization parameter <sup>(5)</sup>	3.2		
$\psi_{JB}$	Junction-to-board characterization parameter <sup>(6)</sup>	57		
$\theta_{JCbott}$	Junction-to-case (bottom) thermal resistance <sup>(7)</sup>	n/a		

(1) 有关传统和全新热度的更多信息，请参阅 *IC 封装热量量* 应用报告（文献号：SPRA953）。

(2) 在 JESD51-2a 描述的环境中，按照 JESD51-7 的规定，在一个 JEDEC 标准高 K 电路板上进行仿真，从而获得自然对流条件下的结至环境热阻抗。

(3) 通过在封装顶部模拟一个冷板测试来获得结至芯片外壳（顶部）的热阻。不存在特定的 JEDEC 标准测试，但可在 ANSI SEMI 标准 G30-88 中找到内容接近的说明。

(4) 按照 JESD51-8 中的说明，通过在配有用于控制 PCB 温度的环形冷板夹具的环境中进行仿真，以获得结至电路板的热阻。

(5) 结至顶部的特征参数，( $\psi_{JT}$ )，估算真实系统中器件的结温，并使用 JESD51-2a（第 6 章和第 7 章）中描述的程序从仿真数据中提取出该参数以便获得  $\theta_{JA}$ 。

(6) 结至电路板的特征参数，( $\psi_{JB}$ )，估算真实系统中器件的结温，并使用 JESD51-2a（第 6 章和第 7 章）中描述的程序从仿真数据中提取出该参数以便获得  $\theta_{JA}$ 。

(7) 通过在外露（电源）焊盘上进行冷板测试仿真来获得结至芯片外壳（底部）热阻。不存在特定的 JEDEC 标准测试，但可在 ANSI SEMI 标准 G30-88 中找到了内容接近的说明。

**RECOMMENDED OPERATING CONDITIONS<sup>(1)</sup>**

		MIN	TYP	MAX	UNIT
$V_{IN}$	Input voltage range, $V_{IN}$	$I_{OUT} \leq 2.5A$	2.5	5.5	V
		$I_{OUT} \geq 2.5A$	2.8	5.5	
$I_{OUT,avg}$	Continuous output current <sup>(1)</sup>			2.5	A
$t_{rf}$	Rising and falling signal transition time at EN, VSEL		30		mV/ $\mu$ s
$T_A$	Operating ambient temperature <sup>(2)</sup>	-40		85	°C
$T_J$	Operating junction temperature	-40		150	°C

(1) Refer to the **APPLICATION INFORMATION** section for further information.

(2) In applications where high power dissipation and/or poor package thermal resistance is present, the maximum ambient temperature may have to be derated. Maximum ambient temperature [ $T_{A(max)}$ ] is dependent on the maximum operating junction temperature [ $T_{J(max)}$ ], the maximum power dissipation of the device in the application [ $P_{D(max)}$ ], and the junction-to-ambient thermal resistance of the part/package in the application ( $\theta_{JA}$ ), as given by the following equation:  $T_{A(max)} = T_{J(max)} - (\theta_{JA} \times P_{D(max)})$

### ELECTRICAL CHARACTERISTICS

Unless otherwise noted, the specification applies for  $V_{IN} = 3.6V$  over an operating ambient temp.  $-40^{\circ}C \leq T_A \leq 85^{\circ}C$ ; Circuit of Parameter Measurement Information section (unless otherwise noted). Typical values are for  $T_A = 25^{\circ}C$ .

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>INPUT</b>						
$V_{IN}$	Input voltage range at $V_{IN}$ , $AV_{IN}$		2.5		5.5	V
$V_{DD}$	I <sup>2</sup> C and registers supply voltage range		1.15		3.6	V
$I_{SD(AVIN)}$	Shutdown current into $AV_{IN}$	EN = LOW, $V_{DD} = 0V$		0.65	5	$\mu A$
$I_{SD(VIN)}$	Shutdown current into $V_{IN}$	EN = LOW, $V_{DD} = 0V$	$T_A = 25^{\circ}C$	0.5	1	$\mu A$
			$T_A = 85^{\circ}C$	1	3	$\mu A$
$I_{SD(VDD)}$	Shutdown current into $V_{DD}$	EN = LOW, I <sup>2</sup> C bus idle		0.01		$\mu A$
$I_Q$	Operating quiescent current into ( $AV_{IN} + V_{IN}$ )	EN = HIGH, $I_{OUT} = 0mA$ , not switching	PFM mode	56		$\mu A$
			Forced PWM mode (Test Mode)	180		$\mu A$
$V_{UVLO}$	Under voltage lock out at $AV_{IN}$	Input voltage falling, EN = High		2.3	2.45	V
		Input voltage rising, EN = Low		1.3		V
$V_{UVLO,HYST(AVIN)}$	Under voltage lock out hysteresis at $AV_{IN}$	Input voltage rising		110		mV
$V_{DD,UVLO}$	Under voltage lock out at $V_{DD}$	Input voltage falling	0.7	0.92	1.1	V
$V_{UVLO,HYST(VDD)}$	Under voltage lock out hysteresis at $V_{DD}$	Input voltage rising		50		mV
$I_{VDD}$	Input current at $V_{DD}$	I <sup>2</sup> C not active		0		$\mu A$
		I <sup>2</sup> C active (r/w)		0.02	1	mA
<b>LOGIC INTERFACE</b>						
$V_{IH}$	High-level input voltage at EN, VSEL		1.2			V
$V_{IL}$	Low-level input voltage at EN, VSEL				0.4	V
$V_{IH,I2C}$	High-level input voltage at SCL, SDA		0.7x $V_{DD}$			V
$V_{IL,I2C}$	Low-level input voltage at SCL, SDA				0.3x $V_{DD}$	V
$I_{LKG}$	Logic input leakage current at EN, VSEL, SDA, SCL	Internal pulldown resistors disabled		0.05		$\mu A$
$R_{PD}$	Pull down resistance at EN, VSEL	Internal pulldown resistors enabled		300		k $\Omega$
	I <sup>2</sup> C clock frequency	Fast mode			400	kHz
		High speed mode			3.4	MHz
<b>POWER SWITCH</b>						
$R_{DS(on)}$	High side MOSFET switch	$V_{IN} = 3.6V$	25	44	75	m $\Omega$
	Low side MOSFET switch	$V_{IN} = 3.6V$	25	32	50	m $\Omega$
$I_{LIMF}$	High side MOSFET forward current limit	$V_{IN} = 3.6V$	4.3	4.9	5.5	A
	Low side MOSFET forward current limit	$V_{IN} = 3.6V$	3.9	4.4	4.9	A
	Low side MOSFET negative current limit	$V_{IN} = 3.6V$ , PWM mode	2.2	2.5	2.9	A
$f_{SW}$	Nominal switching frequency	PWM mode		2.5		MHz
$T_{JEW}$	Die temperature early warning			120		$^{\circ}C$
$T_{JSD}$	Thermal shutdown			150		$^{\circ}C$
$T_{JSD,HYST}$	Thermal shutdown hysteresis			20		$^{\circ}C$
$t_{ON,min}$	Minimum on time			120		ns

**ELECTRICAL CHARACTERISTICS (continued)**

Unless otherwise noted, the specification applies for  $V_{IN} = 3.6V$  over an operating ambient temp.  $-40^{\circ}C \leq T_A \leq 85^{\circ}C$ ; Circuit of Parameter Measurement Information section (unless otherwise noted). Typical values are for  $T_A = 25^{\circ}C$ .

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>OUTPUT</b>						
$V_{OUT}$	Output voltage range	10mV increments	0.5		1.77	V
	Output voltage accuracy	$V_{IN} = 2.8V \dots 5.5V$ $V_{OUT} = 0.5V \dots 1.77V$ No load, Forced PWM, $V_{OUT} = [0.77V, 1.3V]$ $T_J = 85^{\circ}C$	-0.5%		+0.5%	
			No load, Forced PWM, $T_J = -40 \dots 150^{\circ}C$	-1%	$\pm 0.5\%$	+1%
	Line regulation	$I_{OUT} = 1A$ , forced PWM		< 0.1		%/V
	Load regulation	$V_{OUT} = 1.2V$ , forced PWM		< 0.05		%/A
$t_{Start}$	Start-up time	Time from active EN to $V_{OUT} = 1.4V$ , $C_{OUT} < 100\mu F$ , RMP[2:0] = 000, $I_{OUT} = 0mA$			1	ms
$R_{Sense}$	Input resistance between Sense+, Sense-			2.2		M $\Omega$
	Ramp timer	RMP[2:0] = 000		32		mV/ $\mu s$
		RMP[2:0] = 001		16		
		RMP[2:0] = 010		8		
		RMP[2:0] = 011		4		
		RMP[2:0] = 100		2		
		RMP[2:0] = 101		1		
		RMP[2:0] = 110		0.5		
		RMP[2:0] = 111		0.25		

**I<sup>2</sup>C INTERFACE TIMING REQUIREMENTS<sup>(1)</sup>**

PARAMETER		TEST CONDITIONS	MIN	MAX	UNIT
f <sub>(SCL)</sub>	SCL clock frequency	Standard mode		100	kHz
		Fast mode		400	kHz
		High-speed mode (write operation), C <sub>B</sub> – 100 pF max		3.4	MHz
		High-speed mode (read operation), C <sub>B</sub> – 100 pF max		3.4	MHz
		High-speed mode (write operation), C <sub>B</sub> – 400 pF max		1.7	MHz
		High-speed mode (read operation), C <sub>B</sub> – 400 pF max		1.7	MHz
t <sub>BUF</sub>	Bus free time between a STOP and START condition	Standard mode	4.7		μs
		Fast mode	1.3		μs
t <sub>HD</sub> , t <sub>STA</sub>	Hold time (repeated) START condition	Standard mode	4		μs
		Fast mode	600		ns
		High-speed mode	160		ns
t <sub>LOW</sub>	Low period of the SCL clock	Standard mode	4.7		μs
		Fast mode	1.3		μs
		High-speed mode, C <sub>B</sub> – 100 pF max	160		ns
		High-speed mode, C <sub>B</sub> – 400 pF max	320		ns
t <sub>HIGH</sub>	High period of the SCL clock	Standard mode	4		μs
		Fast mode	600		ns
		High-speed mode, C <sub>B</sub> – 100 pF max	60		ns
		High-speed mode, C <sub>B</sub> – 400 pF max	120		ns
t <sub>SU</sub> , t <sub>STA</sub>	Setup time for a repeated START condition	Standard mode	4.7		μs
		Fast mode	600		ns
		High-speed mode	160		ns
t <sub>SU</sub> , t <sub>DAT</sub>	Data setup time	Standard mode	250		ns
		Fast mode	100		ns
		High-speed mode	10		ns
t <sub>HD</sub> , t <sub>DAT</sub>	Data hold time	Standard mode	0	3.45	μs
		Fast mode	0	0.9	μs
		High-speed mode, C <sub>B</sub> – 100 pF max	0	70	ns
		High-speed mode, C <sub>B</sub> – 400 pF max	0	150	ns
t <sub>RCL</sub>	Rise time of SCL signal	Standard mode	20 + 0.1 C <sub>B</sub>	1000	ns
		Fast mode	20 + 0.1 C <sub>B</sub>	300	ns
		High-speed mode, C <sub>B</sub> – 100 pF max	10	40	ns
		High-speed mode, C <sub>B</sub> – 400 pF max	20	80	ns
t <sub>RCL1</sub>	Rise time of SCL signal after a repeated START condition and after an acknowledge bit	Standard mode	20 + 0.1 C <sub>B</sub>	1000	ns
		Fast mode	20 + 0.1 C <sub>B</sub>	300	ns
		High-speed mode, C <sub>B</sub> – 100 pF max	10	80	ns
		High-speed mode, C <sub>B</sub> – 400 pF max	20	160	ns
t <sub>FCL</sub>	Fall time of SCL signal	Standard mode	20 + 0.1 C <sub>B</sub>	300	ns
		Fast mode	20 + 0.1 C <sub>B</sub>	300	ns
		High-speed mode, C <sub>B</sub> – 100 pF max	10	40	ns
		High-speed mode, C <sub>B</sub> – 400 pF max	20	80	ns
t <sub>RDA</sub>	Rise time of SDA signal	Standard mode	20 + 0.1 C <sub>B</sub>	1000	ns
		Fast mode	20 + 0.1 C <sub>B</sub>	300	ns
		High-speed mode, C <sub>B</sub> – 100 pF max	10	80	ns
		High-speed mode, C <sub>B</sub> – 400 pF max	20	160	ns

(1) S/M = standard mode; F/M = fast mode

I<sup>2</sup>C INTERFACE TIMING REQUIREMENTS<sup>(1)</sup> (continued)

PARAMETER	TEST CONDITIONS	MIN	MAX	UNIT
t <sub>FDA</sub> Fall time of SDA signal	Standard mode	20 + 0.1 C <sub>B</sub>	300	ns
	Fast mode	20 + 0.1 C <sub>B</sub>	300	ns
	High-speed mode, C <sub>B</sub> – 100 pF max	10	80	ns
	High-speed mode, C <sub>B</sub> – 400 pF max	20	160	ns
t <sub>SU</sub> , t <sub>STO</sub> Setup time for STOP condition	Standard mode	4		μs
	Fast mode	600		ns
	High-speed mode	160		ns
C <sub>B</sub> Capacitive load for SDA and SCL			400	pF

I<sup>2</sup>C TIMING DIAGRAMS

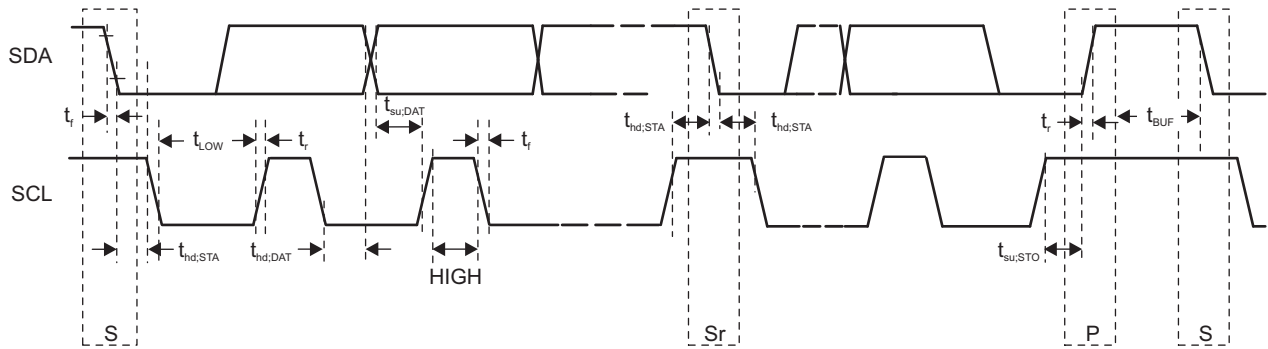
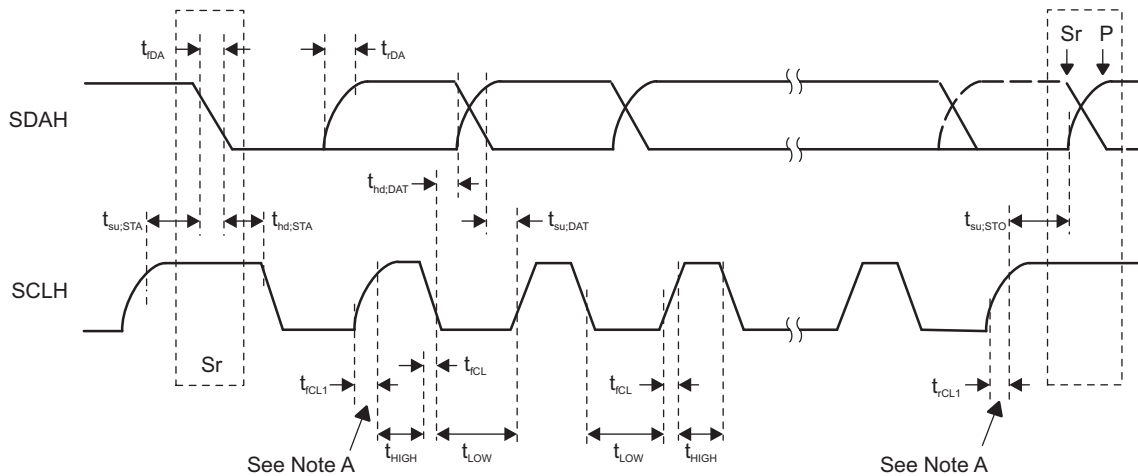


Figure 1. Serial Interface Timing for F/S Mode



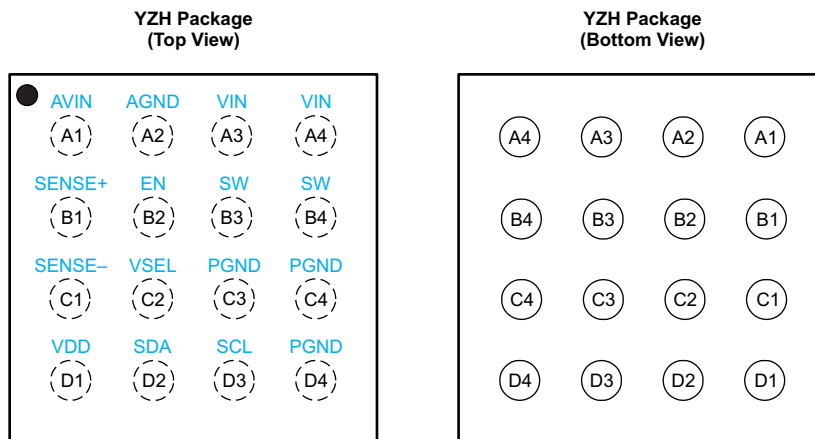
= MCS Current Source Pull-Up  
 = R<sub>(p)</sub> Resistor Pull-Up

Note A: First rising edge of the SCLH signal after Sr and after each acknowledge bit.

Figure 2. Serial Interface Timing for H/S Mode

## DEVICE INFORMATION

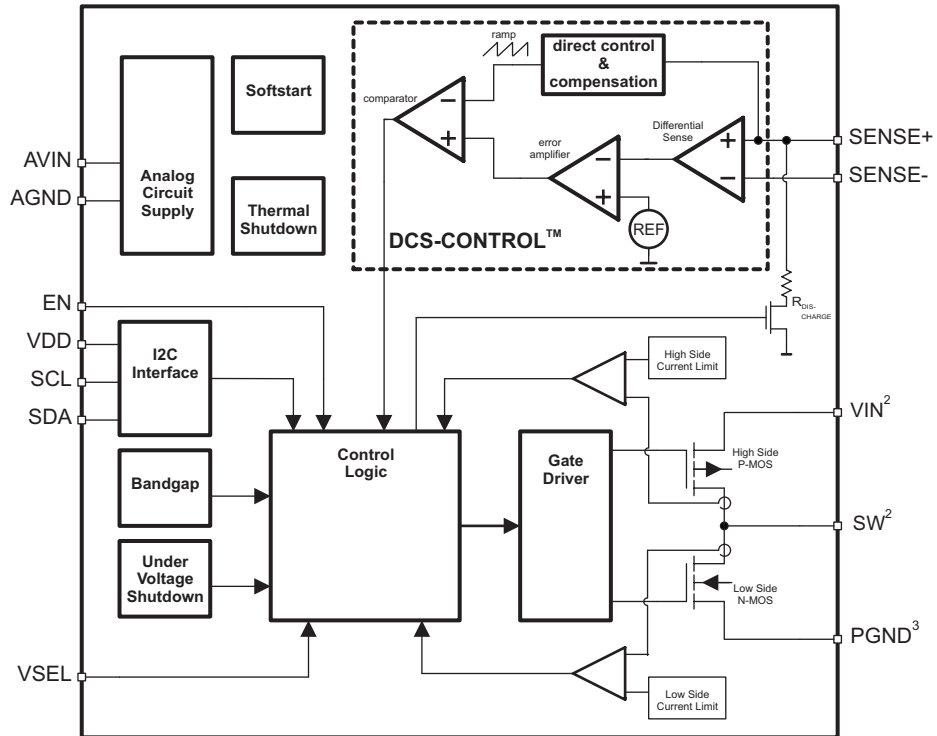
### PIN ASSIGNMENTS



### PIN FUNCTIONS

PIN		I/O	DESCRIPTION
NAME	NO.		
AVIN	A1	I	Analog Supply Voltage Input.
AGND	A2	–	Analog Ground Connection.
EN	B2	I	Device Enable Logic Input. Logic HIGH enables the device, logic LOW disables the device and turns it into shutdown. The pin must be terminated to either HIGH or LOW if the internal pull down resistor is deactivated.
VDD	D1	I	I <sup>2</sup> C Logic and Registers supply voltage. For resetting the internal registers, this connection must be pulled below its UVLO level.
SCL	D3	I/O	I <sup>2</sup> C clock signal.
SDA	D2	I/O	I <sup>2</sup> C data signal.
VSEL	C2	I	Output Settings Selection Logic Input. Predefined register settings can be chosen for setting output voltage and mode. The pin must be terminated to logic HIGH or LOW if the internal pull down resistor is deactivated.
SW	B3	–	Inductor connection
	B4		
SENSE+	B1	I	Positive Output Voltage Remote Sense. Must be connected closest to the load supply node.
SENSE–	C1	I	Negative Output Voltage Remote Sense. Must be connected closest to the load ground node.
VIN	A4	I	Power Supply Voltage Input.
	A3		
PGND	C3	–	Power Ground Connection.
	C4		
	D4		

FUNCTIONAL BLOCK DIAGRAM



## TYPICAL CHARACTERISTICS

Table 1. Table of Graphs

			FIGURE		
$\eta$	Efficiency	vs. Output Current (Power Save and Forced PWM Mode)	$V_{OUT} = 1.5V$	Figure 3	
			$V_{OUT} = 1.2V$	Figure 4	
			$V_{OUT} = 0.9V$	Figure 5	
			$V_{OUT} = 0.6V$	Figure 6	
		vs. Input Voltage (Power Save and Forced PWM Mode)	$I_{OUT} = 4000mA$	Figure 7	
			$I_{OUT} = 1000mA$	Figure 8	
			$I_{OUT} = 100mA$	Figure 9	
			$I_{OUT} = 10mA$	Figure 10	
	$V_O$	DC Output Voltage	vs. Output Current (Power Save and Forced PWM Mode)	$V_{OUT} = 1.5V, T_A = 25^\circ C$	Figure 11
				$V_{OUT} = 1.2V, T_A = 25^\circ C$	Figure 12
$V_{OUT} = 0.9V, T_A = 25^\circ C$				Figure 13	
$V_{OUT} = 0.6V, T_A = 25^\circ C$				Figure 14	
	Startup	Into No Load	$V_{OUT} = 0.5V, I_{OUT} = 0mA$	Figure 15	
			$V_{OUT} = 1.5V, I_{OUT} = 0mA$	Figure 16	
		Into Load	$V_{OUT} = 0.5V, I_{OUT} = 1000mA$	Figure 17	
			$V_{OUT} = 1.5V, I_{OUT} = 1000mA$	Figure 18	
Switching Wave forms	$L = 1\mu H$	$I_{OUT} = 10mA$	Figure 19		
		$I_{OUT} = 200mA$	Figure 20		
		$I_{OUT} = 1000mA$	Figure 21		
		$I_{OUT} = 4000mA$	Figure 22		
	$L = 0.47\mu H$	$I_{OUT} = 10mA$	Figure 23		
		$I_{OUT} = 200mA$	Figure 24		
		$I_{OUT} = 1000mA$	Figure 25		
		$I_{OUT} = 4000mA$	Figure 26		
Output Voltage Ramp Control	Transition 0.5V .. 1.5V	$I_{OUT} = 0mA$	Figure 27		
		$I_{OUT} = 1000mA$	Figure 28		
Load Transient Response	$L = 1\mu H$	$I_{OUT} = 50mA$ to 200mA	Figure 29		
		$I_{OUT} = 200mA$ to 1000mA	Figure 30		
		$I_{OUT} = 2500mA$ to 4000mA	Figure 31		
	$L = 0.47\mu H$	$I_{OUT} = 50mA$ to 200mA	Figure 32		
		$I_{OUT} = 200mA$ to 1000mA	Figure 33		
		$I_{OUT} = 2500mA$ to 4000mA	Figure 34		
Line Transient Response		$V_{IN} = 3.6$ to 4.2V, $I_{OUT} = 3500mA$	Figure 35		
$I_{SD(VIN)}, I_{SD(AVIN)}$	Shutdown Current at AVIN and VIN	vs. Input Voltage	$T_A = [-40^\circ C, 25^\circ C, 125^\circ C]$	Figure 36	
$I_Q$	Operating Quiescent Current	vs. Input Voltage	$T_A = [-40^\circ C, 25^\circ C, 125^\circ C]$ , auto PFM/PWM	Figure 37	
$f_{SW}$	Switching Frequency	vs. Output Current	$V_{OUT} = 1.2V$	Figure 38	
$I_{LIM}$	Current Limit	vs. Input Voltage		Figure 39	
$I_{OUT}$	Maximum DC Output current	vs. Input Voltage	$V_{OUT} = [0.6V, 0.9V, 1.2V, 1.5V]$	Figure 40	

TYPICAL CHARACTERISTICS (continued)

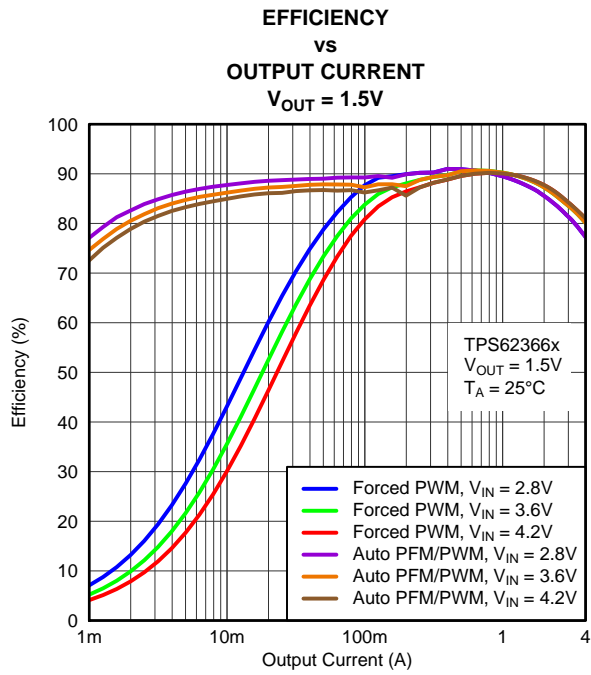


Figure 3.

G001

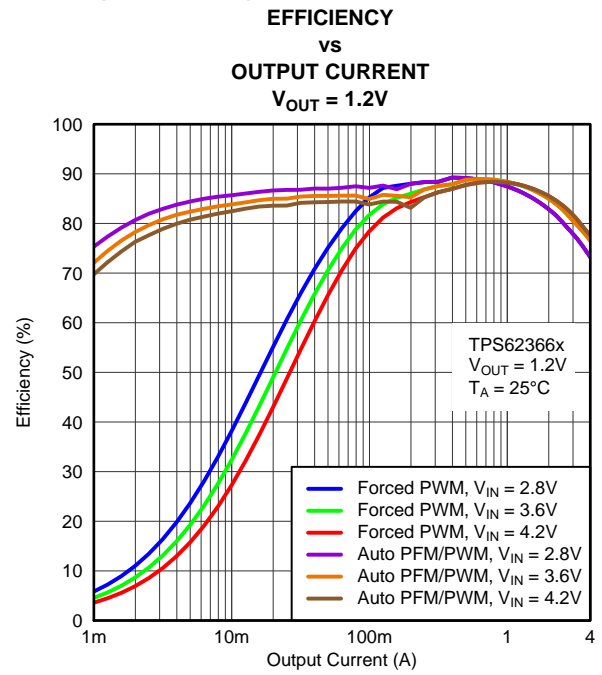


Figure 4.

G002

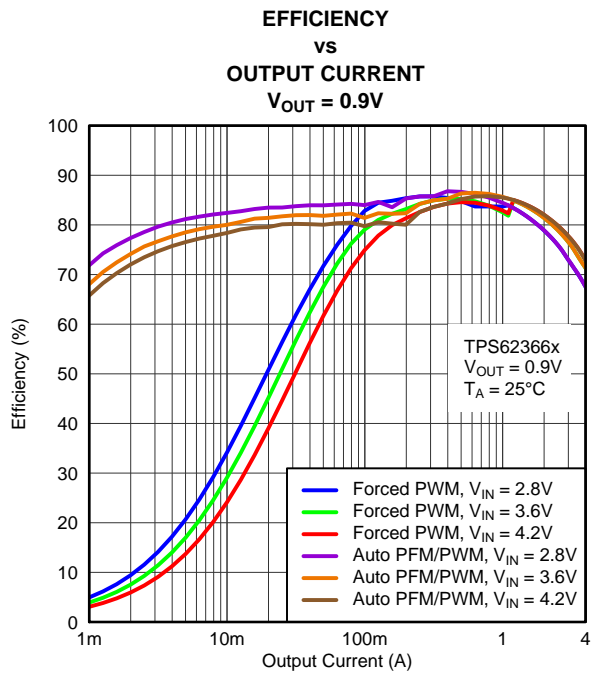


Figure 5.

G003

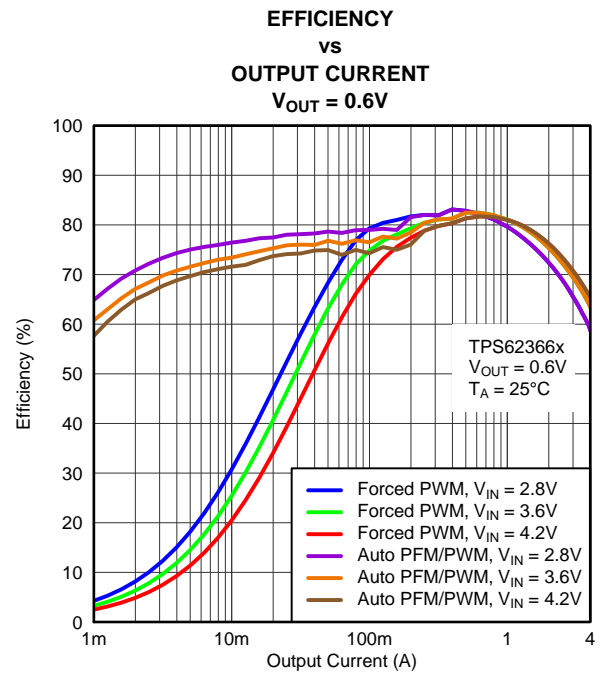


Figure 6.

G004

**TYPICAL CHARACTERISTICS (continued)**

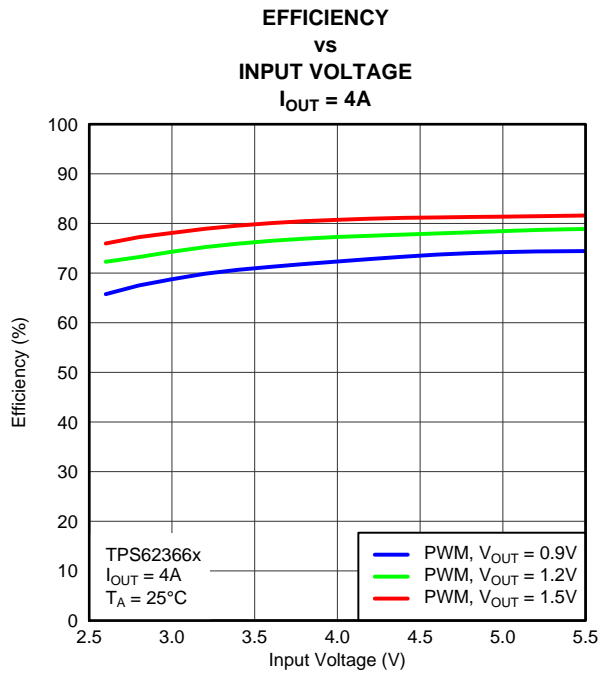


Figure 7.

G005

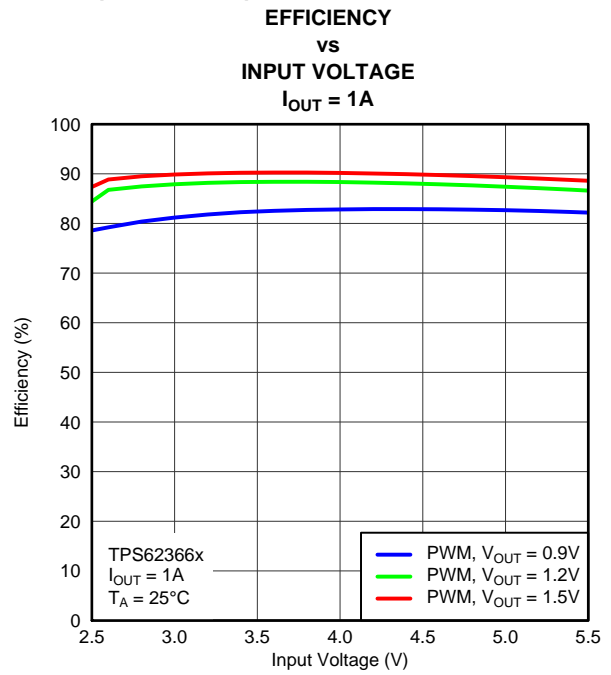


Figure 8.

G006

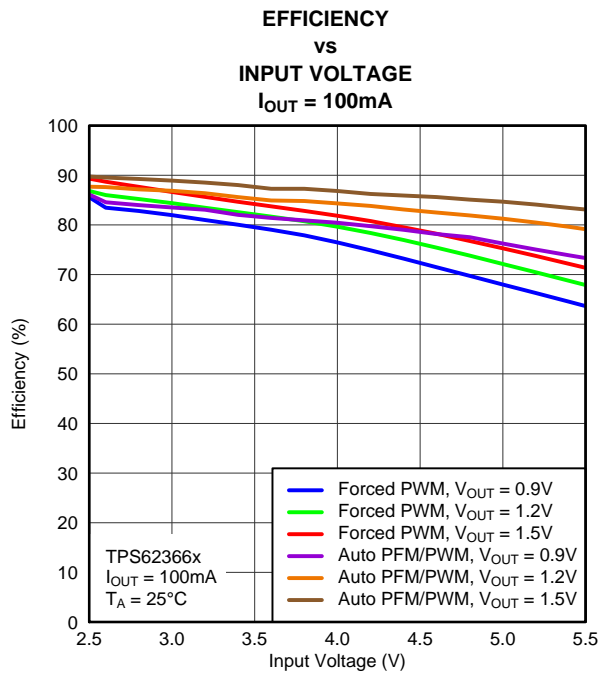


Figure 9.

G007

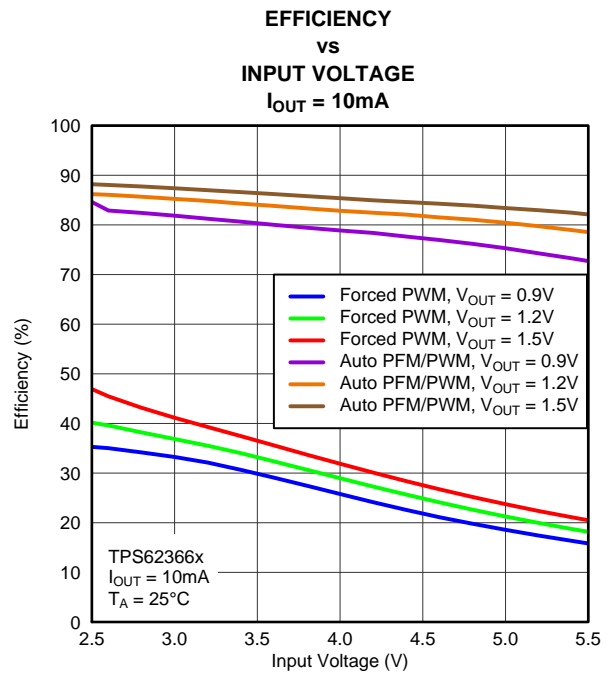


Figure 10.

G008

TYPICAL CHARACTERISTICS (continued)

DC OUTPUT VOLTAGE vs OUTPUT CURRENT  
V<sub>OUT</sub> = 1.5V

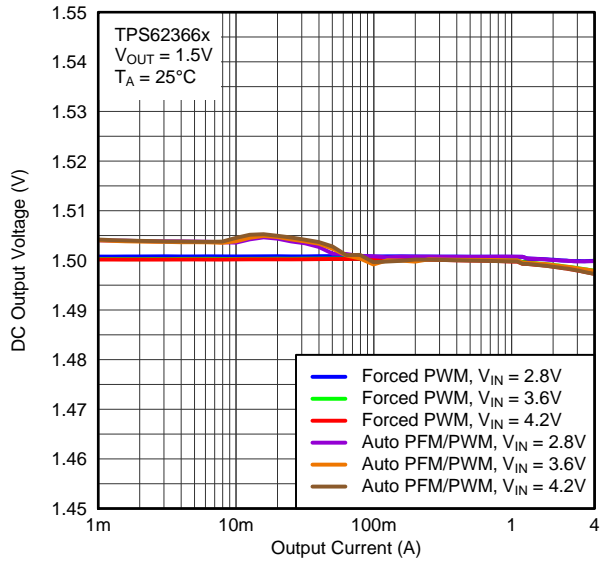


Figure 11.

G009

DC OUTPUT VOLTAGE vs OUTPUT CURRENT  
V<sub>OUT</sub> = 1.2V

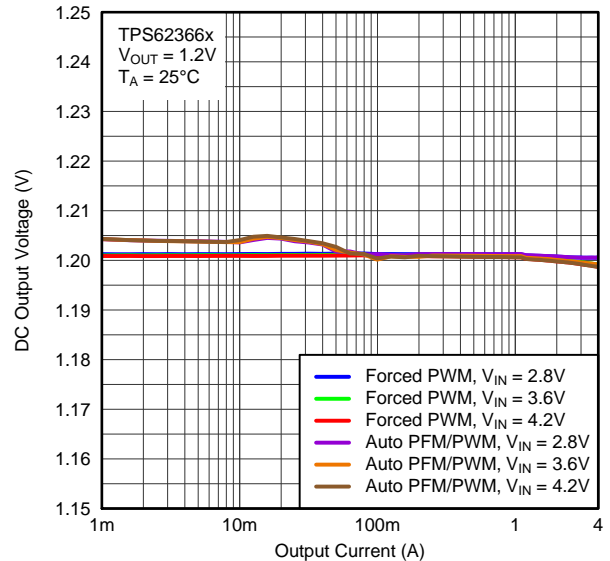


Figure 12.

G010

DC OUTPUT VOLTAGE vs OUTPUT CURRENT  
V<sub>OUT</sub> = 0.9V

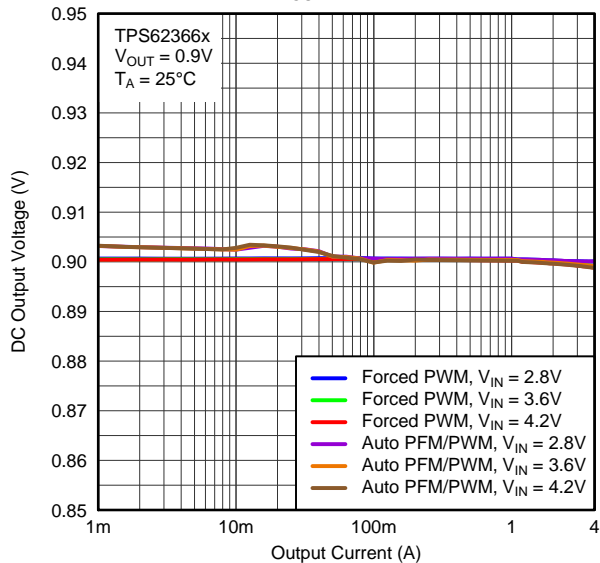


Figure 13.

G011

DC OUTPUT VOLTAGE vs OUTPUT CURRENT  
V<sub>OUT</sub> = 0.6V

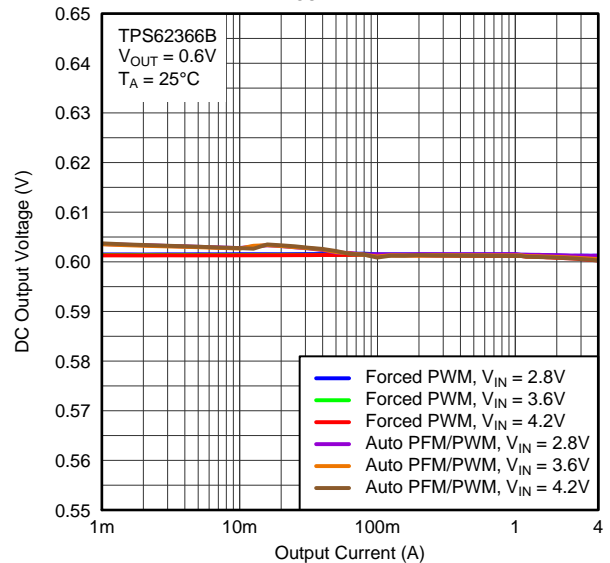
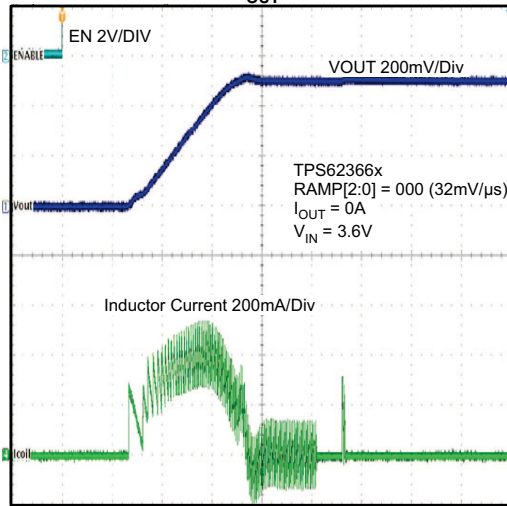


Figure 14.

G012

**TYPICAL CHARACTERISTICS (continued)**

**STARTUP INTO NO LOAD**  
**V<sub>OUT</sub> = 0.5V**

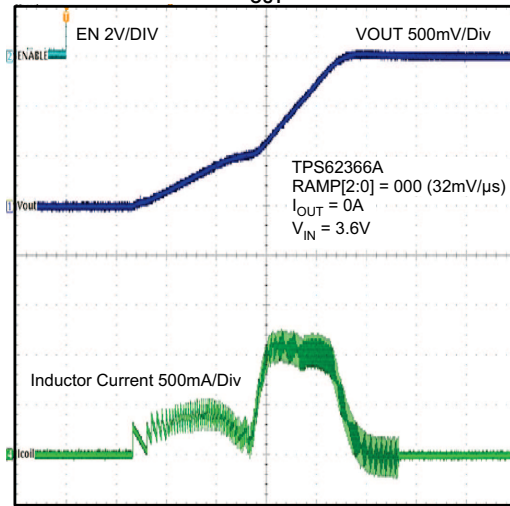


Time Base - 20μs/Div

**Figure 15.**

G013

**STARTUP INTO NO LOAD**  
**V<sub>OUT</sub> = 1.5V**

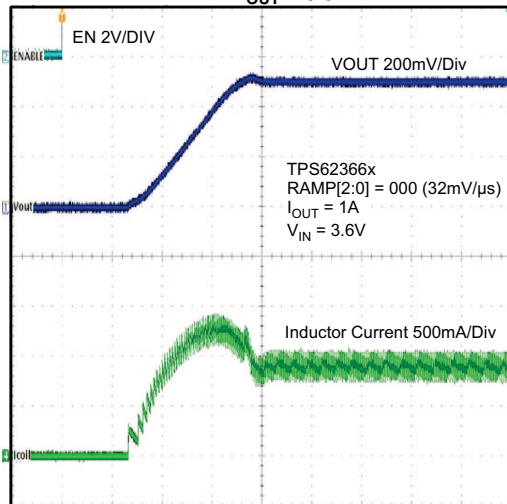


Time Base - 20μs/Div

**Figure 16.**

G014

**STARTUP INTO LOAD**  
**V<sub>OUT</sub> = 0.5V**

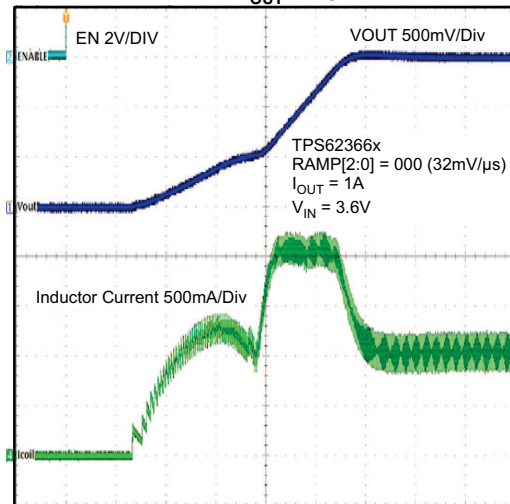


Time Base - 20μs/Div

**Figure 17.**

G015

**STARTUP INTO LOAD**  
**V<sub>OUT</sub> = 1.5V**



Time Base - 20μs/Div

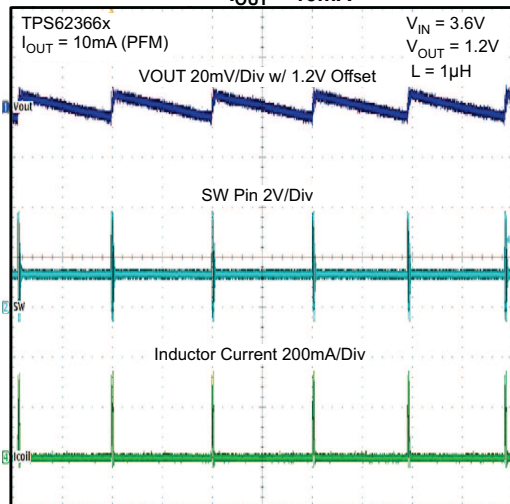
**Figure 18.**

G016

TYPICAL CHARACTERISTICS (continued)

SWITCHING WAVE FORMS

$I_{OUT} = 10mA$



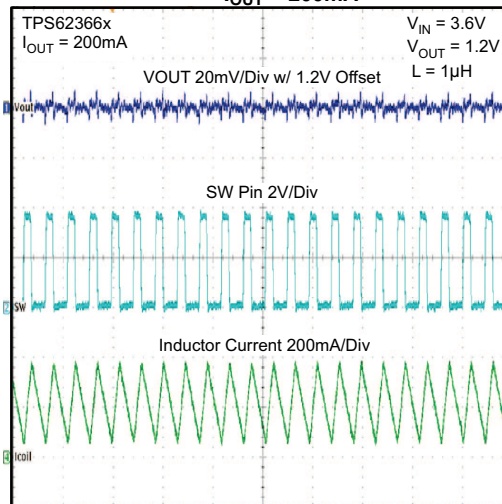
Time Base - 20µs/Div

Figure 19.

G017

SWITCHING WAVE FORMS

$I_{OUT} = 200mA$



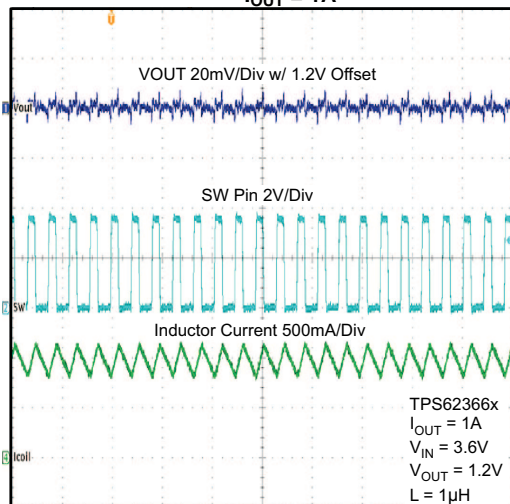
Time Base - 1µs/Div

Figure 20.

G018

SWITCHING WAVE FORMS

$I_{OUT} = 1A$



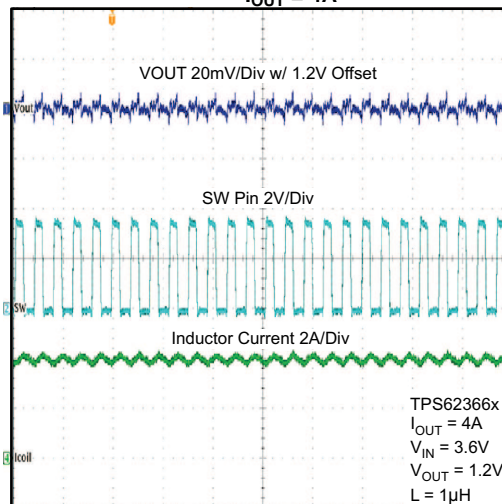
Time Base - 1µs/Div

Figure 21.

G019

SWITCHING WAVE FORMS

$I_{OUT} = 4A$



Time Base - 1µs/Div

Figure 22.

G020

TYPICAL CHARACTERISTICS (continued)

SWITCHING WAVE FORMS  
I<sub>OUT</sub> = 10mA

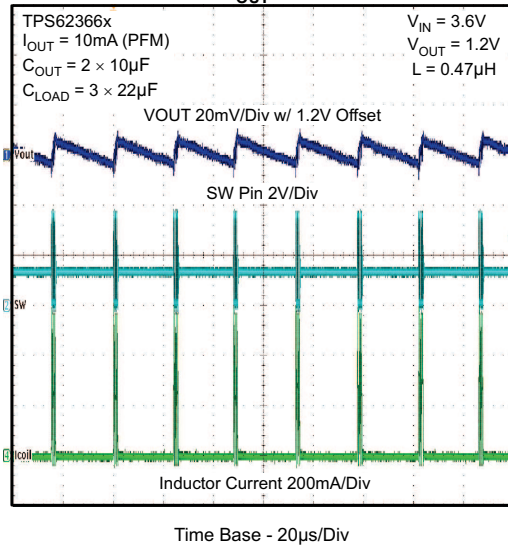


Figure 23.

G037

SWITCHING WAVE FORMS  
I<sub>OUT</sub> = 200mA

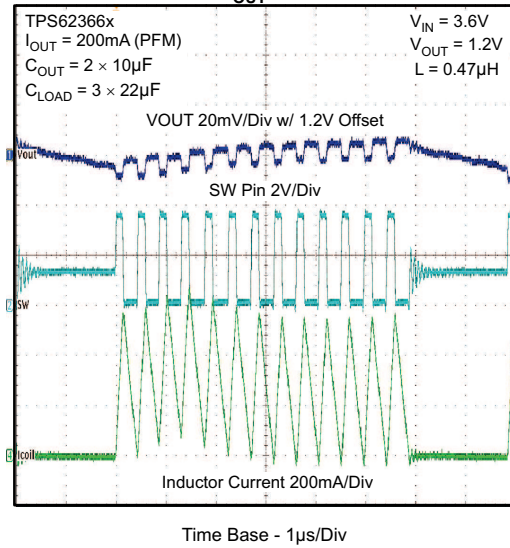


Figure 24.

G038

SWITCHING WAVE FORMS  
I<sub>OUT</sub> = 1A

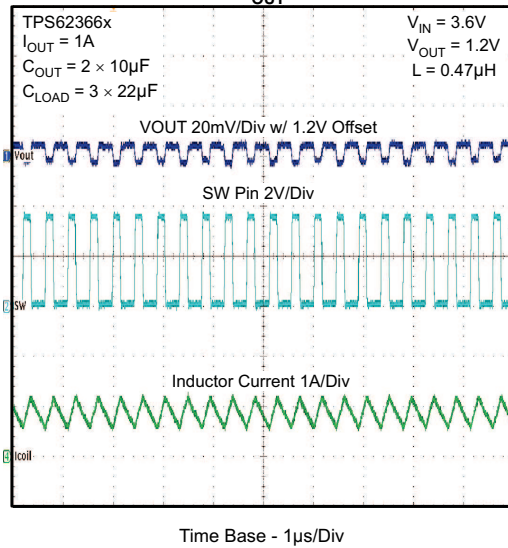


Figure 25.

G039

SWITCHING WAVE FORMS  
I<sub>OUT</sub> = 4A

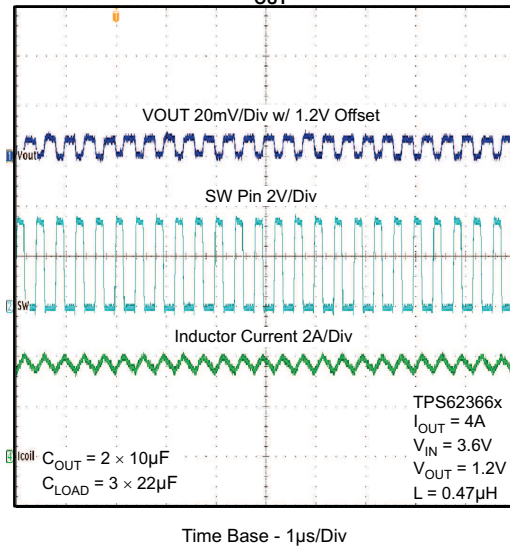
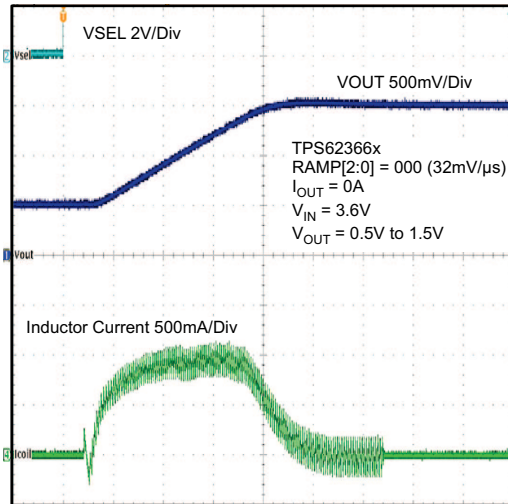


Figure 26.

G040

TYPICAL CHARACTERISTICS (continued)

OUTPUT VOLTAGE RAMP CONTROL  
NO LOAD

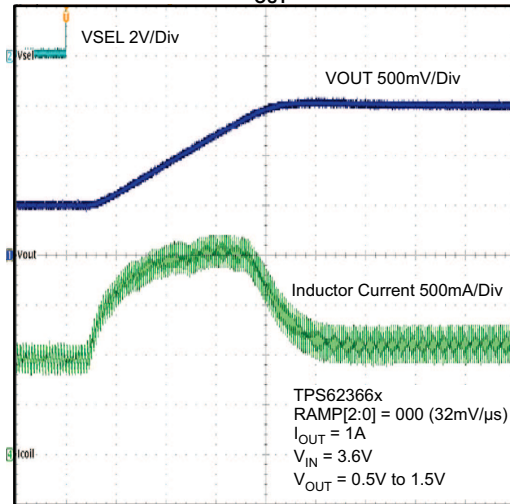


Time Base - 10μs/Div

Figure 27.

G021

OUTPUT VOLTAGE RAMP CONTROL  
I<sub>OUT</sub> = 1A

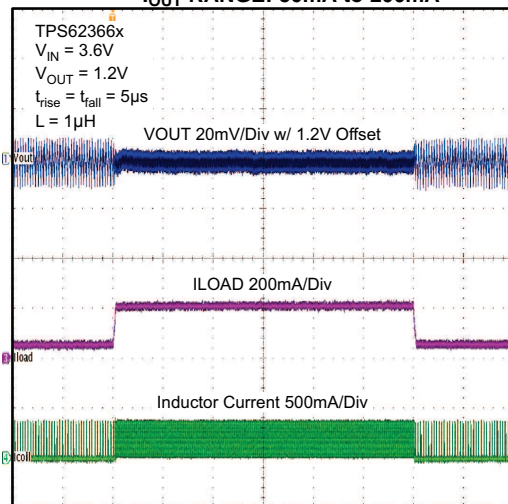


Time Base - 10μs/Div

Figure 28.

G022

LOAD TRANSIENT RESPONSE  
I<sub>OUT</sub> RANGE: 50mA to 200mA

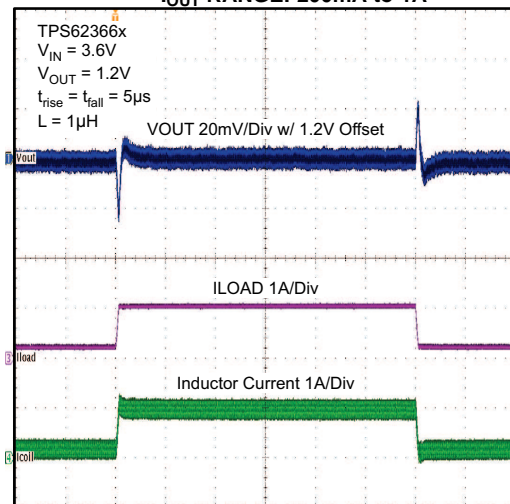


Time Base - 100μs/Div

Figure 29.

G023

LOAD TRANSIENT RESPONSE  
I<sub>OUT</sub> RANGE: 200mA to 1A



Time Base - 100μs/Div

Figure 30.

G024

TYPICAL CHARACTERISTICS (continued)

LOAD TRANSIENT RESPONSE  
I<sub>OUT</sub> RANGE: 2.5A to 4A

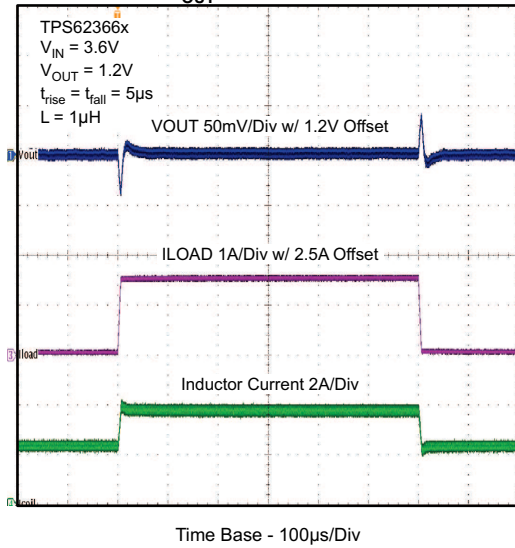


Figure 31.

G025

LOAD TRANSIENT RESPONSE  
I<sub>OUT</sub> RANGE: 50mA to 200mA

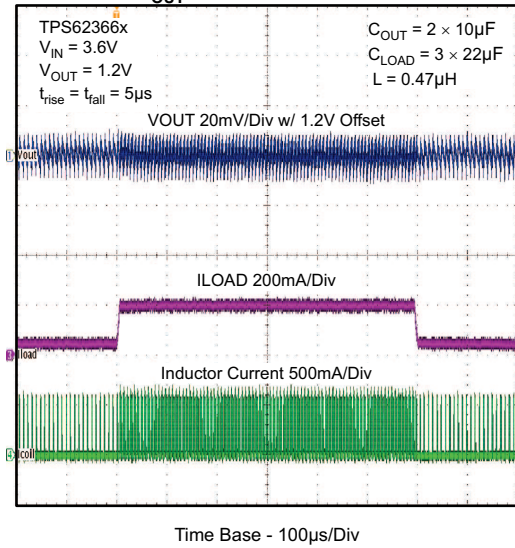


Figure 32.

G041

LOAD TRANSIENT RESPONSE  
I<sub>OUT</sub> RANGE: 200mA to 1A

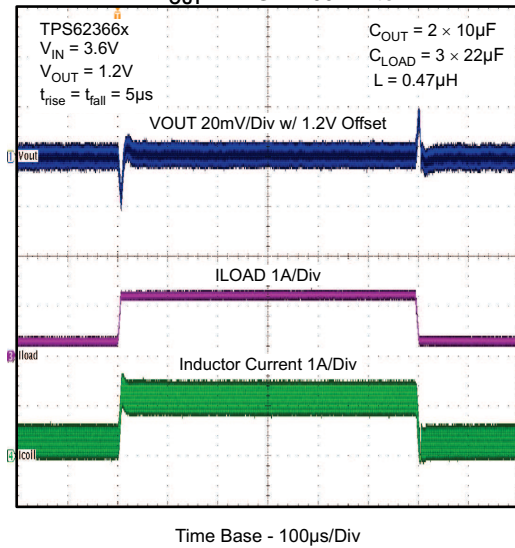


Figure 33.

G042

LOAD TRANSIENT RESPONSE  
I<sub>OUT</sub> RANGE: 2.5A to 4A

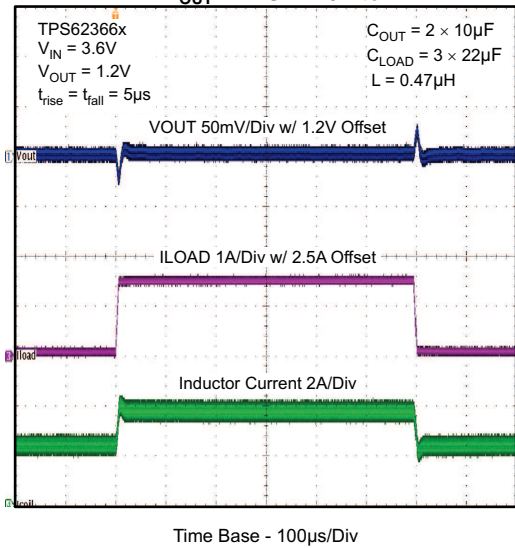


Figure 34.

G043

TYPICAL CHARACTERISTICS (continued)

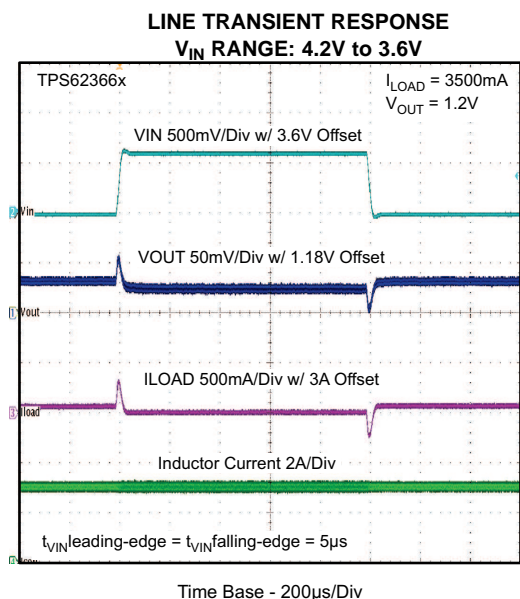


Figure 35.

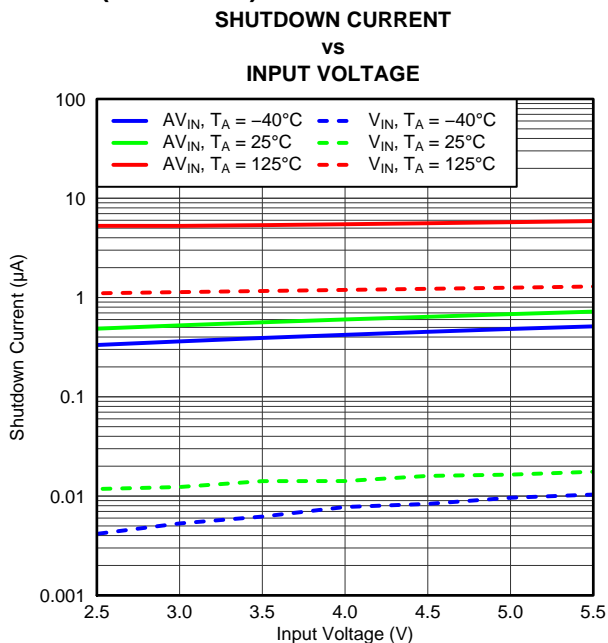


Figure 36.

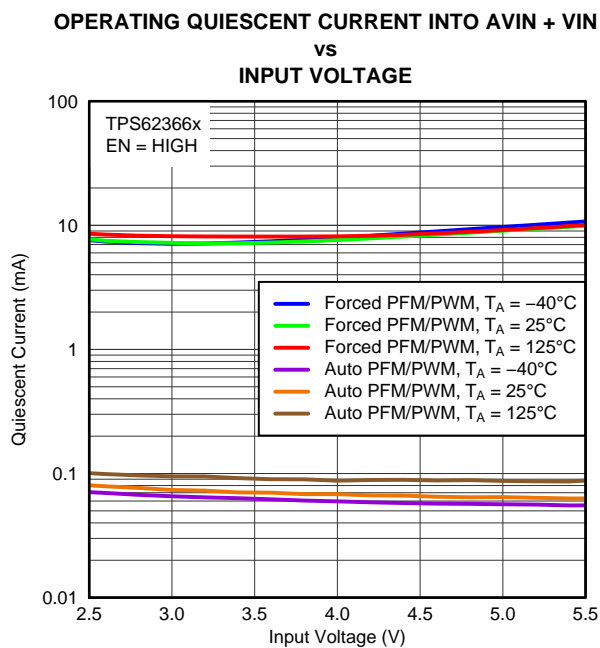


Figure 37.

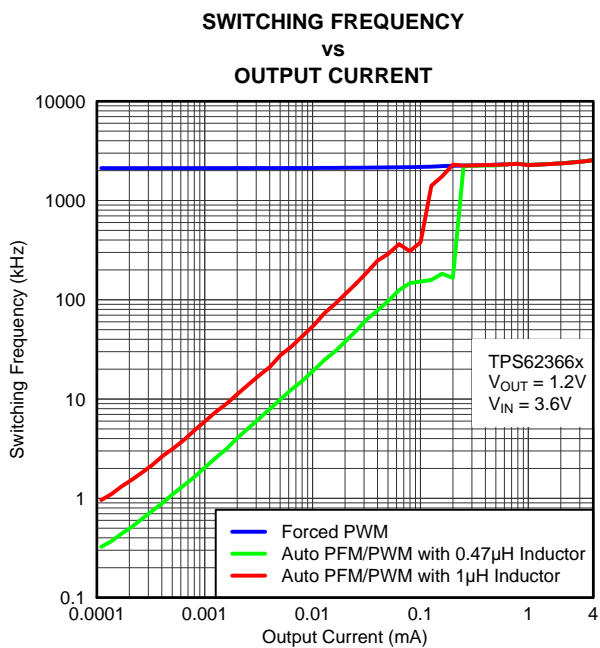


Figure 38.

**TYPICAL CHARACTERISTICS (continued)**

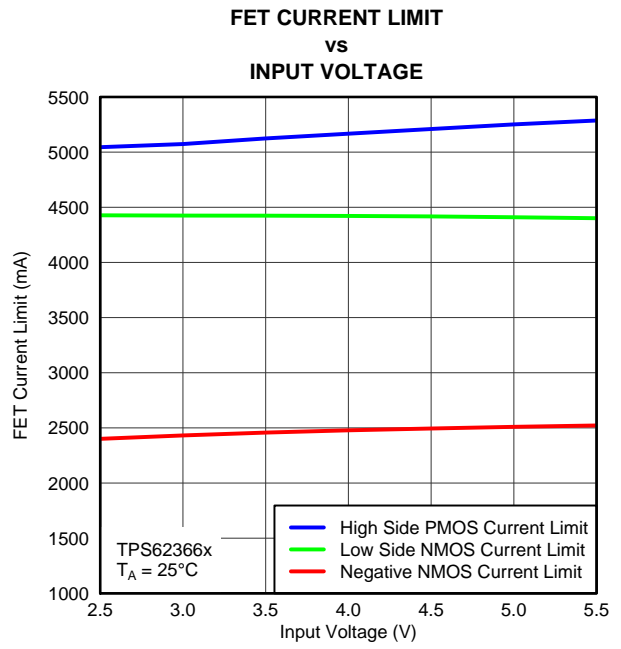


Figure 39.

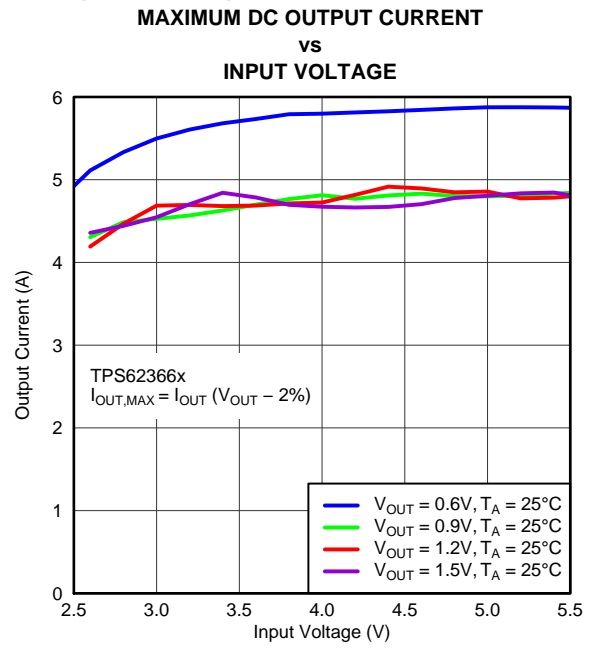
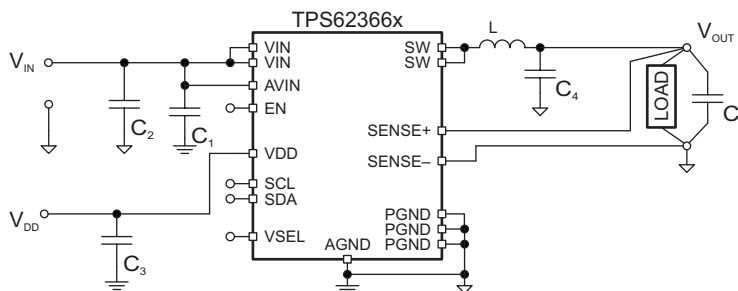


Figure 40.

**PARAMETER MEASUREMENT INFORMATION**

**Table 2. List of Components**

REFERENCE	DESCRIPTION	MANUFACTURER	SETUP
TPS62366x	4A Processor Supply with I <sup>2</sup> C Compatible Interface and Remote Sense, 2.076 mm x 2.076 mm x 0.625mm	Texas Instruments	All Typical Characteristics Figures 3-40
C <sub>1</sub> , C <sub>3</sub>	0.1 μF, Ceramic, 10V, X5R	Standard	
C <sub>2</sub>	10 μF, Ceramic, 6.3V, X5R	Standard	
L	1 μH, 4 mm x 4 mm x 2.1 mm	Coilcraft (XFL4020-102ME1.0)	1 μH Setup: Typical Characteristics Figures 3-22, 27- 31, 36-40
C <sub>4</sub>	10 μF, Ceramic, 6.3V, X5R	Standard	
C <sub>L</sub>	Load Capacitors, 2x10 μF + 4.7μF, Ceramic, 6.3V, X5R	Standard	0.47 μH Setup: Typical Characteristics Figures 23-26, 32-34
C <sub>4</sub>	2 x 10 μF, Ceramic, 6.3V, X5R	Standard	
C <sub>L</sub>	Load Capacitors, 3x22 μF, Ceramic, 6.3V, X5R	Standard	
L	0.47 μH, 4 mm x 4 mm x 1.5 mm	Coilcraft (XFL4015-471MEC)	

## DETAILED DESCRIPTION

The TPS62366x are a family of high-frequency synchronous step down dc-dc converter optimized for battery-powered portable applications. With an input voltage range of 2.5V to 5.5V, common battery technologies are supported.

The device provides up to 4A peak load current, operating at 2.5MHz typical switching frequency.

The devices convert to an output voltage range of 0.5V to 1.77V, programmable via I<sup>2</sup>C interface in 10mV steps.

The TPS62366x supports low-voltage DSPs and processor cores in smart-phones and handheld computers, including latest submicron processes and their retention modes and addresses digital voltage scaling technologies such as SmartReflex™.

Output Voltages and Modes can be fully programmed via I<sup>2</sup>C. To address different performance operating points and/or startup conditions, the device offers two output voltage / mode presets which can be chosen via a dedicated VSEL pin allowing simple and zero latency output voltage transition.

The devices focus on a high output voltage accuracy. The fully differential sensing and the DCS-Control™ architecture achieve precise static and dynamic, transient output voltage regulation. This accounts for stable processor operation. Output voltage security margins can be kept small, resulting in an increased overall system efficiency.

The TPS62366x devices offer high efficiency step down conversion. The area of highest efficiency is extended towards low output currents to increase the efficiency while the processor is operating in retention mode, as well as towards highest output currents reducing the power loss. This addresses the power profile of processors. High efficiency conversion is required for low output currents to support the retention modes of processors, resulting in an increased battery on-time. To address the processor maximum performance operating points with highest output currents, high efficiency conversion is enabled as well to save the battery on-time and reduce input power.

The robust architecture and multiple safety features allow perfect system integration.

The 2mm x 2mm package and the low number of required external components lead to a tiny solution size of approximately less than 25 mm<sup>2</sup>.

## OPERATION

The TPS62366x synchronous switched mode power converters are based on DCS-Control™, an advanced regulation topology, that combines the advantages of hysteretic, voltage mode and current mode control architectures.

While a comparator stage provides excellent load transient response, an additional voltage loop ensures high DC accuracy as well. The TPS62366x compensates ground shifts at the load by the differentially sensing the output voltage at the point of load.

The internal ramp generator adds information about the load current and fast output voltage changes. The internally compensated regulation network achieves fast and stable operation with low ESR capacitors.

The DCS-Control™ topology supports PWM (Pulse Width Modulation) mode for medium and heavy load conditions and a Power Save Mode at light loads. During PWM mode it operates at its nominal switching frequency in continuous conduction mode. This frequency is typically about 2.5MHz with a controlled frequency variation depending on the input voltage. As the load current decreases, the converter enters Power Save Mode to sustain high efficiency down to light loads. The transition from PWM to Power Save Mode is seamless and avoids output voltage transients.

The TPS62366x family offers both excellent DC voltage and superior load transient regulation, combined with very low output voltage ripple, minimizing interference with RF circuits.

## ENABLING AND DISABLING THE DEVICE

The device is enabled by setting the EN input to a logic high. Accordingly, a logic low disables the device. If the device is enabled, the internal power stage starts switching and regulates the output voltage to the programmed threshold. The EN input must be terminated, unless the internal pull down resistor is activated.

The I<sup>2</sup>C interface is operable when VDD and AVIN are present, regardless of the state of the EN pin.

If the device is disabled by pulling the EN to a logic low, the output capacitor can actively be discharged. Per default, this feature is disabled. Programming the EN\_DISC bit to a logic high discharges the output capacitor via a typ. 300Ω path on the SENSE+ pin.

## SOFT START

The device incorporates an internal soft start circuitry that controls the ramp up of the output voltage after enabling the device. This circuitry eliminates inrush current to avoid excessive voltage drops of primary cells and rechargeable batteries with high internal impedance.

During soft start, the output voltage is monotonically ramped up to the minimum programmable output voltage. After reaching this threshold, the output voltage is further increased following the slope as programmed in the ramp rate settings (see [RAMP RATE CONTROLLING](#)) until reaching the programmed output voltage. Once the nominal voltage is reached, regular operation continues.

The device is able to start into a pre biased output capacitor as well.

## PROGRAMMING THE OUTPUT

The TPS62366x devices offer two similar registers to program the output. A dedicated hardware input pin (VSEL) is implemented for choosing the active register. The logic state of the VSEL pin selects the register whose settings are present at the output. The VSEL pin must be terminated, unless the internal pull-down resistor is activated.

The registers have a certain initial default value (see [Table 3](#)) and can be readjusted via I<sup>2</sup>C during operation.

This allows a simple transition between two output options by triggering the dedicated input pin. At the same time since the presets can be readjusted during operation, this offers highest flexibility.

**Table 3. Output Presets**

VSEL PIN	PRESET	I <sup>2</sup> C REGISTER	DEFAULT OPERATION MODE	DEFAULT OUTPUT VOLTAGE [V]	
				TPS62366A	TPS62366B
0	SET0	0x00h – see <a href="#">Table 11</a> and <a href="#">Table 12</a>	Power Save Mode	1.20	0.96
1	SET1	0x01h – see <a href="#">Table 13</a> and <a href="#">Table 14</a>	Power Save Mode	1.16	1.40

Via the I<sup>2</sup>C interface and/or the two preset options, the following output parameters can be changed:

- Output voltage from 0.5V to 1.77V with 10 mV granularity
- Mode of operation: Power Save Mode or forced PWM mode

The slope for transition between different output voltages (Ramp Rate) can be changed via I<sup>2</sup>C as well. The slope applies for all presets globally. See [RAMP RATE CONTROLLING](#) for further details.

Since the output parameters can be changed by a dedicated pin for selecting presets and by I<sup>2</sup>C, the following use scenarios are feasible:

- Control the device via VSEL pin only, after programming the presets, to choose and change within the programmed settings.
- Program via I<sup>2</sup>C only. The dedicated VSEL pin has a fixed connection. Changes are conducted by changing the preset values of the active register.
- Dedicated VSEL pin and I<sup>2</sup>C mixed operation. The non active preset might be changed. The VSEL pin is used for the transition to the new output condition. Changes within an active preset via I<sup>2</sup>C are feasible as well.

## DYNAMIC VOLTAGE SCALING

The output voltage can be adjusted dynamically. Each of the two output registers can be programmed individually by setting OV[6:0] in the SET0 and SET1 registers.

**Table 4. TPS62366x Output Voltage Settings for Registers SET0 and SET1**

REGISTERS: SET0, SET1, SET2, SET3	
OV[D6:D0]	OUTPUT VOLTAGE
000 0000	500 mV
000 0001	510 mV
000 0010	520 mV
000 0011	530 mV
...	...
111 1101	1750 mV
111 1110	1760 mV
111 1111	1770 mV

If the output voltage is changed at the active register (selected by the VSEL status), these changes apply after the I<sup>2</sup>C command is sent.

## POWER SAVE MODE AND FORCED PWM MODE

The TPS62366x devices feature a Power Save Mode to gain efficiency at light output current conditions. The device automatically transitions in both directions between pulse width modulation (PWM) operation at high load and pulse frequency modulation (PFM) operation at light load current. This maintains high efficiency at both light and heavy load currents. In PFM Mode, the device generates single switching pulses when required to maintain the programmed output voltage.

The transition into and out of Power Save Mode happens within the entire regulation scheme and is seamless in both directions.

The output current, at which the device transitions from PWM to PFM operation can be estimated as follows:

$$I_{OUT,TRANS} = \frac{V_{IN} - V_{OUT}}{2} \times \frac{V_{OUT}}{V_{IN}} \times \frac{1}{(f \times L)} \quad (1)$$

With:

- V<sub>IN</sub> = Input voltage
- V<sub>OUT</sub> = Output Voltage
- f = Switching frequency, typ. 2.5 MHz
- L = Inductance (0.47uH - 1uH nominal)

The TPS62366x is optimized for low output voltage ripple. Therefore, the peak inductor current in PFM mode is kept small and can be calculated as follows:

$$I_{L,PFM,peak} = \frac{t_{ON}}{L} \times (V_{IN} - V_{OUT}) \quad (2)$$

And:

$$t_{ON} = \frac{V_{OUT}}{V_{IN}} \times 350ns + 20ns \quad (3)$$

With:

- V<sub>IN</sub> = Input Voltage
- V<sub>OUT</sub> = Output Voltage
- t<sub>ON</sub> = On-time of the High Side FET, from [Equation 3](#)
- L = Inductance

The TPS62366x offers a forced PWM mode as well. In this mode, the converter is forced in PWM mode even at light load currents. This comes with the benefit that the converter is operating with lower output voltage ripple. Compared to the PFM mode, the efficiency is lower during light load currents.

According to the output voltage, the Power Save Mode / forced PWM Mode can be programmed individually for each preset via I<sup>2</sup>C by setting the MODE0 and MODE1 bit D7. Table 3 shows the factory presets after enabling the I<sup>2</sup>C. For additional flexibility, the Power Save Mode can be changed at a preset that is currently active.

## RAMP RATE CONTROLLING

If the output voltage is changed, the TPS62366x actively controls the voltage ramp rate during the transition. An internal oscillator is embedded for high timing precision.

Figure 41 shows the operation principle. If the output voltage changes, the device changes the output voltage by adjusting through discrete steps with a programmable ramp rate resulting in a corresponding transition time. The connected output capacitor flattens the steps.

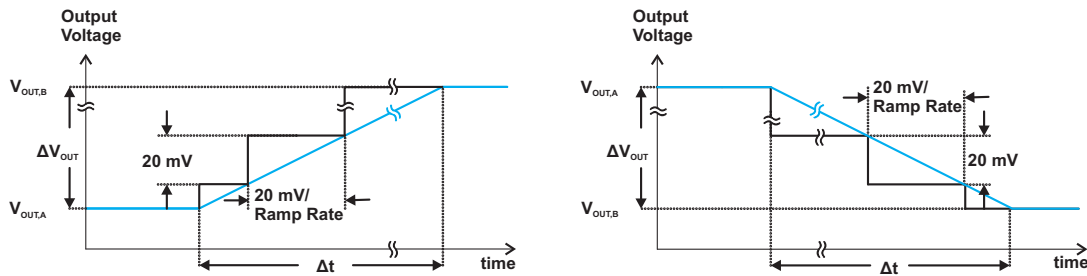


Figure 41. Ramp Up and Down

The ramp up/down slope can be programmed via I<sup>2</sup>C interface (see Table 5).

Table 5. Ramp Rates

RMP [2:0]	RAMP RATE	
	[mV/μs]	[μs/10mV]
000	32	0.3125
001	16	0.625
010	8	1.25
011	4	2.5
100	2	5
101	1	10
110	0.5	20
111	0.25	40

For a transition of the output voltage from V<sub>OUT,A</sub> to V<sub>OUT,B</sub> and vice versa, the resulting ramp up/down slope can be calculated as

$$\frac{\Delta V_{OUT}}{\Delta t} = 32 \frac{\text{mV}}{\mu\text{s}} \frac{1}{2^{(RMP[2-0])_2}} \quad (4)$$

If the device is operating in forced PWM Mode, the device actively controls both the ramp up and down slope.

If Power Save Mode is activated, the ramp up phase follows the programmed slope.

To force the output voltage to follow the ramp down slope in Power Save Mode, the RAMP\_PFM bit needs to be set. This forces the converter to follow the ramp down slope during PFM operation as well.

If the RAMP\_PFM bit is not set in Power Save Mode, the slope can be less at low output currents since the device does not actively source energy back from the output capacitor to the input or it might be sharper at high output currents since the output capacitor is discharged quickly.

The TPS62366x ramps taking 20mV steps with a final 10mV step, if required, for reaching the target output voltage.

While the output voltage setpoint is changed in a digital stair step fashion, the output voltage change is linear due to the output capacitor whose voltage cannot change instantaneously.

## SAFE OPERATION AND PROTECTION FEATURES

### Inductor Current Limit

The inductor current limiting prevents the device from drawing high inductor current and excessive current from the battery. Excessive current might occur with a shorted/saturated inductor or a heavy load/shorted output circuit condition.

The incorporated inductor peak current limit measures the current while the high side power MOSFET is turned on. Once the current limit is tripped, the high side MOSFET is turned off and the low side MOSFET is turned on to ramp down the inductor current. This prevents high currents to be drawn from the battery.

Once the low side MOSFET is on, the low side forward current limit keeps the low side MOSFET on until the current through it decreases below the low side forward current limit threshold.

The negative current limit acts if current is flowing back to the battery from the output. It works differently in PWM and PFM operation. In PWM operation, the negative current limit prevents excessive current from flowing back through the inductor to the battery, preventing abnormal voltage conditions at the switching node. In PFM operation, a zero current limits any power flow back to the battery by preventing negative inductor current.

### Die Temperature Monitoring and Over Temperature Protection

The TPS62366x offers two stages of die temperature monitoring and protection.

The Early Warning Monitoring Feature monitors the device temperature and provides the host an indication that the die temperature is in the higher range. If the device's junction temperature,  $T_J$ , exceeds 120°C typical, the TJEW bit is set high. To avoid the thermal shutdown being triggered, the current drawn from the TPS62366x should be reduced at this early stage.

The Over Temperature Protection feature disables the device if the temperature increases due to heavy load and/or high ambient temperature. It monitors the device die temperature and, if required, triggers the device into shutdown until the die temperature falls sufficiently.

If the junction temperature,  $T_J$ , exceeds 150°C typical, the device goes into thermal shutdown. In this mode, the power stage is turned off. During thermal shutdown, the I<sup>2</sup>C interface remains operable. All register values are kept.

For the thermal shutdown, a hysteresis of 20°C typical is implemented allowing the device to cool after the shutdown is triggered. Once the junction temperature  $T_J$  cools down to 130°C typical, the device resumes operation.

If a thermal shutdown has occurred, the TJTS bit is latched and remains a logic high as long as VDD and AVIN are present and until the bit is reset by the host.

### Input Under Voltage Protection

The input under voltage protection is implemented in order to prevent operation of the device for low input voltage conditions. If the device is enabled, it prevents the device from switching if AVIN falls below the under voltage lock out threshold. If the AVIN under voltage protection threshold is tripped, the device goes into under voltage shutdown instantaneously, turning the power stage off and resetting all internal registers. The input under voltage protection is also implemented on the VDD input. If the VDD under voltage protection threshold is tripped, the device resets all internal registers.

A under voltage lock out hysteresis of  $V_{UVLO,HYST(AVIN)}$  at AVIN and  $V_{UVLO,HYST(VDD)}$  at VDD is implemented.

The I<sup>2</sup>C compatible interface remains fully functional if AVIN and VDD are present. If the under voltage lock out of AVIN or VDD is triggered during operation, all internal registers are reset to their default values. [Figure 42](#) shows the UVLO block diagram.

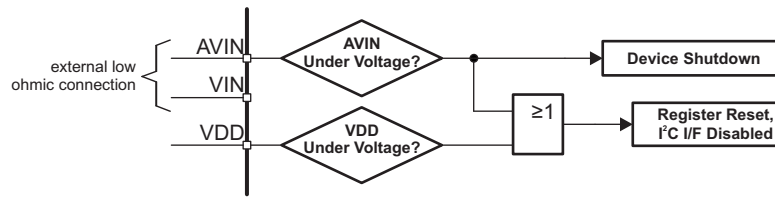


Figure 42. UVLO State Chart

By connecting VIN and AVIN to the same potential, VIN is included in the under voltage monitoring. If a low pass input filter is applied at AVIN (not mandatory for the TPS62366x), the delay and shift in the voltage level can be calculated by taking the typical quiescent current  $I_Q$  at AVIN. As an example, for  $I_Q$  and  $10\Omega$  series resistance, this results in a minimal static shift of approx.  $560\mu\text{V}$ .

VIN and AVIN must be connected to the same source for proper device operation.

## APPLICATION INFORMATION

### I<sup>2</sup>C INTERFACE

#### Serial Interface Description

I<sup>2</sup>C is a 2-wire serial interface developed by Philips Semiconductor (see I<sup>2</sup>C-Bus Specification, Version 2.1, January 2000). The bus consists of a data line (SDA) and a clock line (SCL) with pull-up structures. When the bus is *idle*, both SDA and SCL lines are pulled high. All the I<sup>2</sup>C compatible devices connect to the I<sup>2</sup>C bus through open drain I/O pins, SDA and SCL. A *master* device, usually a micro controller or a digital signal processor, controls the bus. The master is responsible for generating the SCL signal and device addresses. The master also generates specific conditions that indicate the START and STOP of data transfer. A *slave* device receives and/or transmits data on the bus under control of the master device.

The TPS62366x device works as a *slave* and supports the following data transfer *modes*, as defined in the I<sup>2</sup>C-Bus Specification:

- Standard mode (100 kbps)
- Fast mode (400 kbps)
- Fast mode plus (1Mbps)
- High-speed mode (3.4 Mbps)

The interface adds flexibility to the power supply solution, enabling most functions to be programmed to new values depending on the instantaneous application requirements. Register contents remain intact as long as VDD and AVIN are present in the specified range. Tripping the under voltage lock out of AVIN or VDD deletes the registers and establishes the default values once the supply is present again.

The data transfer protocol for standard and fast modes is exactly the same; therefore, they are referred to as F/S-mode in this document. The protocol for high-speed mode is different from F/S-mode, and it is referred to as HS-mode. The TPS62366x device supports 7-bit addressing. 10-bit addressing and general call addressing are not supported.

Table 6 shows the TPS62366x devices and their assigned I<sup>2</sup>C addresses.

Table 6. I<sup>2</sup>C Address

DEVICE OPTION	I <sup>2</sup> C ADDRESS	
	HEXADECIMAL CODED	BINARY CODED
TPS62366A	(0x60) <sub>HEX</sub>	(110 0000) <sub>2</sub>
TPS62366B	(0x60) <sub>HEX</sub>	(110 0000) <sub>2</sub>

#### F/S-Mode Protocol

The master initiates data transfer by generating a start condition. The start condition is when a high-to-low transition occurs on the SDA line while SCL is high, as shown in Figure 43. All I<sup>2</sup>C-compatible devices should recognize a start condition.

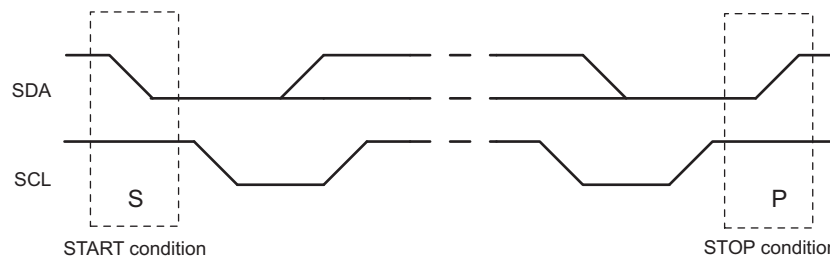


Figure 43. START and STOP Conditions

The master then generates the SCL pulses, and transmits the 7-bit address and the read/write direction bit R/W on the SDA line. During all transmissions, the master ensures that data is valid. A valid data condition requires the SDA line to be stable during the entire high period of the clock pulse (see Figure 44). All devices recognize the address sent by the master and compare it to their internal fixed addresses. Only the slave device with a matching address generates an acknowledge (see Figure 45) by pulling the SDA line low during the entire high period of the ninth SCL cycle. Upon detecting this acknowledge, the master knows that communication link with a slave has been established.

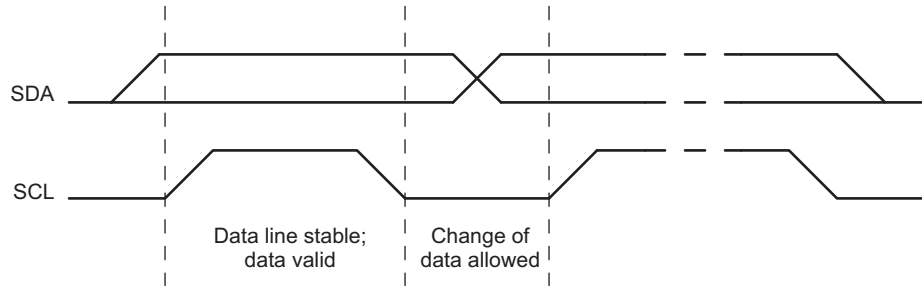


Figure 44. Bit Transfer on the Serial Interface

The master generates further SCL cycles to either transmit data to the slave (R/W bit 1) or receive data from the slave (R/W bit 0). In either case, the receiver needs to acknowledge the data sent by the transmitter. So an acknowledge signal can either be generated by the master or by the slave, depending on which one is the receiver. 9-bit valid data sequences consisting of 8-bit data and 1-bit acknowledge can continue as long as necessary.

To signal the end of the data transfer, the master generates a stop condition by pulling the SDA line from low to high while the SCL line is high (see Figure 43). This releases the bus and stops the communication link with the addressed slave. All I<sup>2</sup>C compatible devices must recognize the stop condition. Upon the receipt of a stop condition, all devices know that the bus is released, and they wait for a start condition followed by a matching address.

Attempting to read data from register addresses not listed in this section results in 00h being read out.

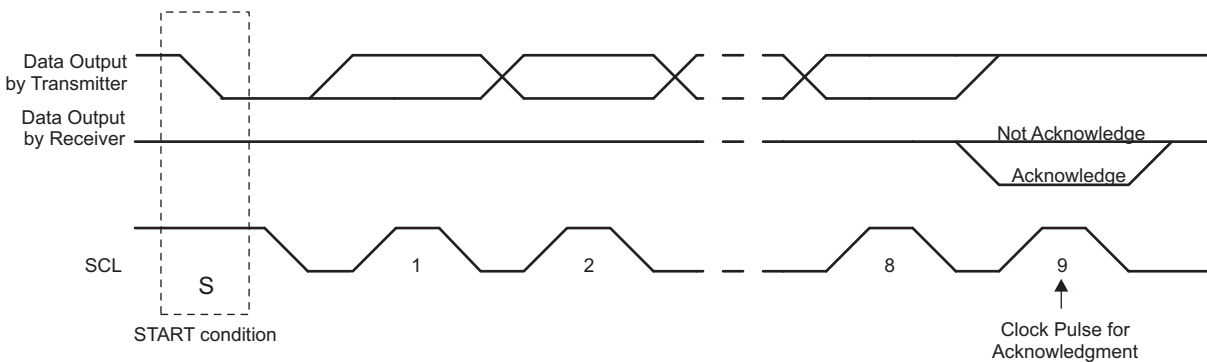


Figure 45. Acknowledge on the I<sup>2</sup>C Bus

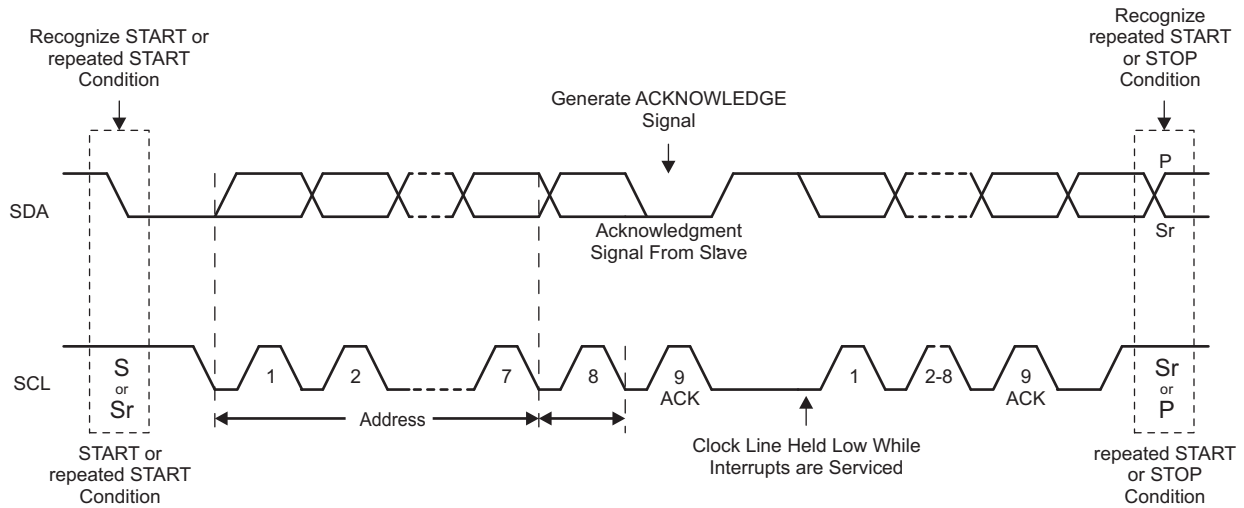


Figure 46. Bus Protocol

**HS-Mode Protocol**

When the bus is idle, both SDA and SCL lines are pulled high by the pull-up devices.

The master generates a start condition followed by a valid serial byte containing HS master code 00001XXX. This transmission is made in F/S-mode at no more than 400 Kbps. No device is allowed to acknowledge the HS master code, but all devices must recognize it and switch their internal setting to support 3.4 Mbps operation.

The master then generates a *repeated start condition* (a repeated start condition has the same timing as the start condition). After this repeated start condition, the protocol is the same as F/S-mode, except that transmission speeds up to 3.4 Mbps are allowed. A stop condition ends the HS-mode and switches all the internal settings of the slave devices to support the F/S-mode. Instead of using a stop condition, repeated start conditions should be used to secure the bus in HS-mode.

Attempting to read data from register addresses not listed in this section results in 00h being read out.

**I<sup>2</sup>C UPDATE SEQUENCE**

The TPS62366x requires a start condition, a valid I<sup>2</sup>C address, a register address byte, and a data byte for a single update. After the receipt of each byte, the TPS62366x device acknowledges by pulling the SDA line low during the high period of a single clock pulse. A valid I<sup>2</sup>C address selects the TPS62366x. The TPS62366x performs an update on the falling edge of the acknowledge signal that follows the LSB byte.

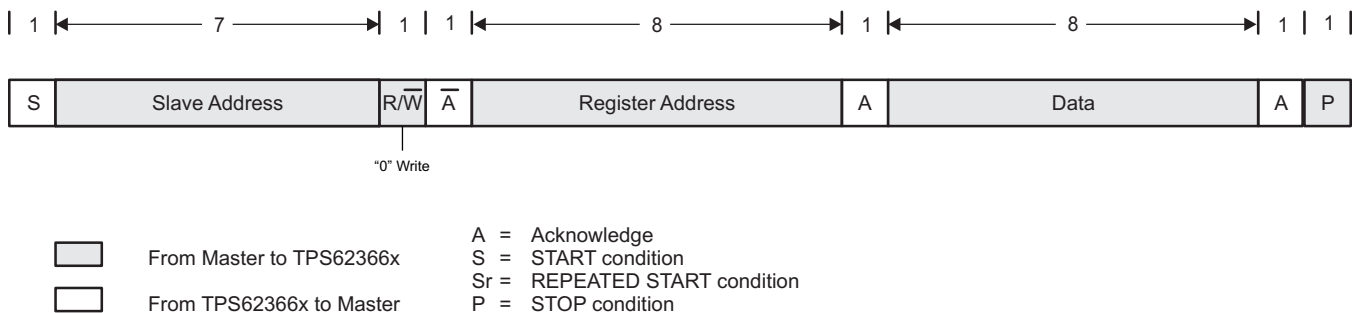


Figure 47. Write Data Transfer Format in F/S-Mode

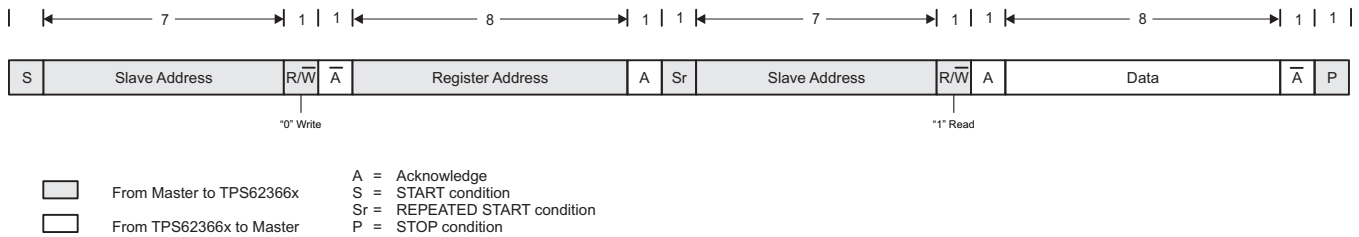


Figure 48. Read Data Transfer Format in F/S-Mode

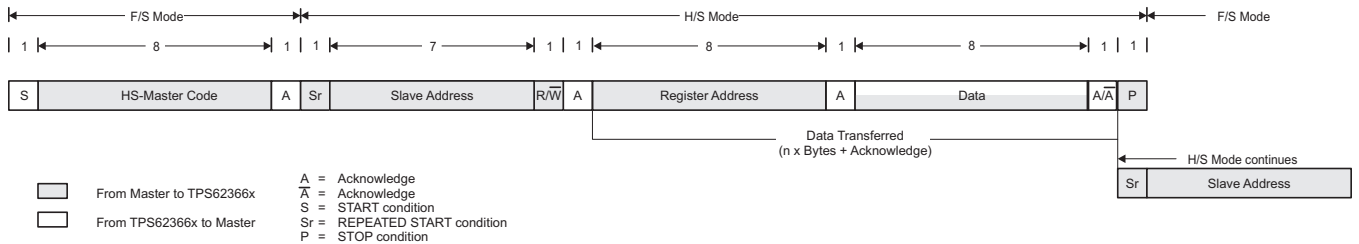


Figure 49. Data Transfer Format in H/S-Mode

### Slave Address Byte

MSB							LSB
X	X	X	X	X	X	A1	A0

The slave address byte is the first byte received following the START condition from the master device.

### Register Address Byte

MSB							LSB
0	0	0	0	0	D2	D1	D0

Following the successful acknowledgment of the slave address, the bus master sends a byte to the TPS62366x, which contains the address of the register to be accessed.

### I<sup>2</sup>C REGISTER RESET

The I<sup>2</sup>C registers can be reset by pulling VDD below the VDD Under Voltage Level,  $V_{DD,UVLO}$ . VDD can be used as a hardware reset function to reset the registers to defaults, if VDD is supplied by a GPIO of the host. The host's GPIO must be capable of driving  $I_{VDD,max}$ .

Refer to the [Input Under Voltage Protection](#) section for details.

### PULL DOWN RESISTORS

The EN and VSEL inputs feature internal pull down resistors to discharge the potential if one of the pins is not connected or is triggered by a high impedance source. See [Figure 50](#). By default, the pull down resistors are enabled.

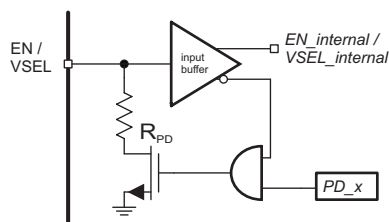


Figure 50. Pull Down Resistors at EN and VSEL pins

If a pin is read as a logic HIGH, its pull down resistor is disconnected dynamically to reduce power consumption. To achieve lowest possible quiescent current or if external pull up/down resistors are employed, the internal pull down resistors can be disabled individually at EN and VSEL by I<sup>2</sup>C programming the registers PD\_EN and PD\_VSEL.

## INPUT CAPACITOR SELECTION

The input capacitor is required to buffer the pulsing current drawn by the device at VIN and reducing the input voltage ripple. The pulsing current is originated by the operation principles of a step down converter.

Low ESR input capacitors are required for best input voltage filtering and minimal interference with other system components. For best performance, ceramic capacitors with a low ESR at the switching frequency are recommended. X7R or X5R type capacitors should be used.

A ceramic input capacitor in the nominal range of C<sub>IN</sub> = 4.7μF to 22μF should be a good choice for most application scenarios. In general, there is no upper limit for increasing the input capacitor.

For typical operation, a 10μF X5R type capacitor is recommended. [Table 7](#) shows a list of recommended capacitors.

**Table 7. List of Recommended Capacitors**

CAPACITANCE [μF]	TYPE	DIMENSIONS L x W x H [mm <sup>3</sup> ]	MANUFACTURER
10	GRM188R60J106M	0603: 1.6 x 0.8 x 0.8	Murata
10	CL10A106MQ8NRNC	0603: 1.6 x 0.8 x 0.8	Samsung
22	GRM188R60G226M	0603: 1.6 x 0.8 x 0.8	Murata
22	CL10A106MQ8NRNC	0603: 1.6 x 0.8 x 0.8	Samsung

## DECOUPLING CAPACITORS AT AVIN, VDD

Noise impacts can be reduced by buffering AVIN and VDD with a decoupling capacitor. It is recommended to buffer AVIN and VDD with a X5R or X7R ceramic capacitor of at least 0.1μF connected between AVIN, AGND and VDD, AGND respectively. The capacitor closest to the pin should be kept small (< 0.22μF) in order to keep a low impedance at high frequencies. In general, there is no upper limit for the total capacitance.

## INDUCTOR SELECTION

The choice of the inductor type and value has an impact on the inductor ripple current, the transition point of PFM to PWM operation, the output voltage ripple and accuracy. The subsections below support for choosing the proper inductor.

### Inductance Value

The TPS62366x is designed for best operation with a nominal inductance value of 1μH.

Inductances down to 0.47μH nominal may be used to improve the load transient behavior or to decrease the total solution size. See [OUTPUT FILTER DESIGN](#) for details.

Depending on the inductance, using inductances lower than 1μH results in a higher inductor current ripple. It can be calculated as:

$$\Delta I_L = V_{OUT} \times \frac{1 - \frac{V_{OUT}}{V_{IN}}}{L \times f} \quad (5)$$

With:

V<sub>IN</sub> = Input Voltage

V<sub>OUT</sub> = Output Voltage

f = Switching frequency, typ. 2.5MHz

L = Inductance

## Inductor Saturation Current

The inductor needs to be selected for its current rating. To pick the proper saturation current rating, the maximum inductor current can be calculated as:

$$I_{L,MAX} = I_{OUT,MAX} + \frac{\Delta I_L}{2} \quad (6)$$

With:

$\Delta I_L$  = Inductor ripple current (see [Equation 5](#))

$I_{OUT,MAX}$  = Maximum output current

Since the inductance can be decreased by saturation effects and temperature impact, the inductor needs to be chosen to have an effective inductance of at least 0.3 $\mu$ H under temperature and saturation effects.

[Table 8](#) shows a list of inductors that have been used with the TPS62366x. Special care needs to be taken for choosing the proper inductor, taking e.g. the load profile into account.

**Table 8. List of Recommended Inductors**

INDUCTANCE [ $\mu$ H]	SATURATION CURRENT RATING <sup>(1)</sup> ( $\Delta I/L \approx 30\%$ , typ) [A]	TEMPERATURE CURRENT RATING <sup>(1)</sup> ( $\Delta T = 40^\circ\text{C}$ , typ) [A]	DIMENSIONS L x W x H [mm <sup>3</sup> ]	DC RESISTANCE [m $\Omega$ typ]	TYPE	MANUFACTURER
1.0	5.4	11.0	4.0 x 4.0 x 2.1	11	XFL4020-102ME1.0	Coilcraft
1.0	4.7	3.6	3.2 x 2.5 x 1.2	34	DFE322512C	Toko
1.0	6.0	4.1	4.4 x 4.1 x 1.2	38	SPM4012	TDK
1.0	4.7	3.8	3.2 x 2.5 x 1.2	35	PILE32251B- 1R0MS-11 <sup>(2)</sup>	Cyntec
1.0	4.5	7.0	4.15 x 4.0 x 1.8	24	PIMB042T-1R0MS- 11	Cyntec
1.0	4.2	3.7	2.5 x 2.0 x 1.2	38	DFE252012R -H- 1R0N <sup>(2)</sup>	Toko
0.47	6.6	11.2	4.0 x 4.0 x 1.5	8	XFL4015-471M	Coilcraft
0.47	5	4.5	2.5 x 2.0 x 1.2	23	PIFE25201B- R47MS-11 <sup>(2)</sup>	Cyntec
0.47	5.2	4.4	2.5 x 2.0 x 1.2	27	DFE252012R -H- R47N <sup>(3)</sup>	Toko

(1) Excessive inductor temperature might result in a further effective inductance drop which might be below or close to the max. current limit threshold,  $I_{LIM,max}$ , depending on the inductor, use case and thermal board design. Proper saturation current rating must be verified, taking into account the use scenario and thermal board layout.

(2) Product preview, release planned for Q3/4 2012. Contact manufacturer for details.

(3) Under development, typ. data might change. Contact manufacturer for schedule and details.

## OUTPUT CAPACITOR SELECTION

The unique hysteretic control scheme allows the use of tiny ceramic capacitors. For best performance, ceramic capacitors with low ESR values are recommended to achieve high conversion efficiency and low output voltage ripple. For stable operation, X7R or X5R type capacitors are recommended.

The TPS62366x is designed to operate with a minimum output capacitor of 10 $\mu$ F for a 1 $\mu$ H inductor and 2x10 $\mu$ F for a 0.47 $\mu$ H inductor, placed at the device's output. In addition, a 0.1 $\mu$ F capacitor can be added to the output to reduce the high frequency content created by a very sudden load change. For stability, an overall maximum output capacitance must not be exceeded. See [OUTPUT FILTER DESIGN](#).

[Table 7](#) shows a list of tested capacitors. The TPS62366x is not designed for use with polymer, tantalum, or electrolytic output capacitors.

## OUTPUT FILTER DESIGN

The inductor and the output capacitors create the output filter. The output capacitors consist of  $C_{OUT}$  and buffer capacitors at the load,  $C_{LOAD}$ . See Figure 51. Buffering the load by ceramic capacitors,  $C_{LOAD}$ , improves the voltage quality at the load input and the dynamic load step behavior. This is especially true if the trace between the TPS62366x and the load is longer than the smallest possible.

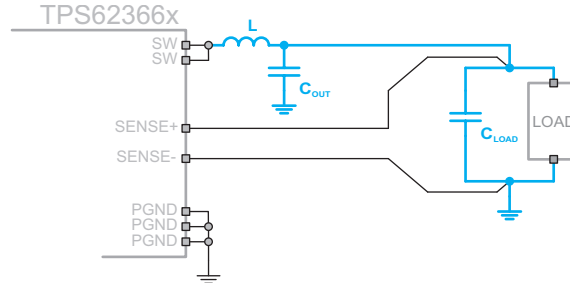


Figure 51. L,  $C_{OUT}$  and  $C_{LOAD}$  Forming the Output Filter

Depending on the chosen inductor value, a certain minimum output capacitor  $C_{OUT}$  must be present. Also depending on the chosen inductor value, a maximum output and buffer capacitor configuration ( $C_{OUT} + C_{LOAD}$ ) must not be exceeded. Figure 52 shows the range of L,  $C_{OUT}$  and  $C_{LOAD}$  that create a stable output filter.

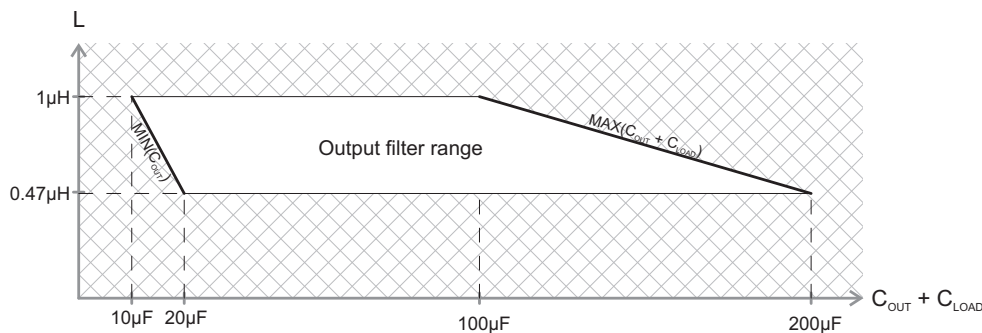


Figure 52. Recommended L,  $C_{OUT}$  and  $C_{LOAD}$  Combinations

Within the allowed output filter range, a certain filter can be chosen to improve further on application specific key parameters.

The choice of the inductance, L, affects the inductor current ripple, output voltage ripple, the PFM to PWM transition point and the PFM operation switching frequency.

The TPS62366x is designed for operation with a nominal inductance value of 1µH. Inductances down to 0.47µH nominal may be used to improve the load transient behavior (see Figure 31 and Figure 34) or to decrease the total solution size. This increases the inductor current ripple (see Equation 5). As a consequence, the output voltage ripple is increased if the output capacitance is kept constant. The increased inductor ripple current also causes higher peak inductor currents (see Equation 6), requiring a higher saturation current rating. Furthermore, the PFM switching frequency is decreased (see Figure 38) and the automatic PFM to PWM transition occurs at a higher output current (see Equation 1).

The choice of the output and buffer capacitance ( $C_{OUT}$  and  $C_{LOAD}$ ) affects the load step behavior, output voltage ripple, PFM switching frequency and output voltage transition time.

A higher output capacitance improves the load step behavior and reduces the output voltage ripple as well as decreasing the PFM switching frequency. For very large output filter combinations, the output voltage might be slower than the programmed ramp rate at voltage transitions (see RAMP RATE CONTROLLING) because of the higher energy stored on the output capacitance. At startup, the time required to charge the output capacitor to 0.5V might be longer. At shutdown, if the output capacitor is discharged by the internal discharge resistor (see ENABLING AND DISABLING THE DEVICE), this requires more time to settle  $V_{OUT}$  down as a consequence of the increased time constant  $T = R_{DISCHARGE} \times (C_{OUT} + C_{LOAD})$ .

For further performance or specific demands, these values might be tweaked. In any case, the loop stability should be checked since the control loop stability might be affected. At light loads, if the device is operating in PFM Mode, choosing a higher value minimizes the voltage ripple resulting in a better DC output accuracy.

## THERMAL AND DEVICE LIFETIME INFORMATION

Implementation of integrated circuits in low-profile and fine-pitch surface-mount packages typically requires special attention to power dissipation. Many system-dependent issues such as thermal coupling, airflow, added heat sinks and convection surfaces, and the presence of other heat-generating components affect the power-dissipation limits of a given component.

Proper PCB layout, focusing on thermal performance, results in lower die temperatures. Wide power traces come with the ability to sink dissipated heat. This can be improved further on multi-layer PCB designs with vias to different layers. Proper This results in reduced junction-to-ambient ( $\theta_{JA}$ ) and junction-to-board ( $\theta_{JB}$ ) thermal resistances and thereby reduces the device junction temperature,  $T_J$ .

The TI reliability requirement for the silicon chip's life time (100K Power-On-Hours at  $T_J = 105^\circ\text{C}$ ) is affected by the junction temperature and the continuously drawn output current. In order to be consistent with the TI reliability requirement for the silicon chips (100000 Power-On-Hours at  $T_J = 105^\circ\text{C}$ ), the average output current  $I_{OUT,avg}$  should not continuously exceed 2550mA so as to prevent electromigration failure in the SW pins solder bumps.

Exceeding  $I_{OUT,avg}$  and/or  $T_{J,max}$  might affect the device reliability by electromigration. Electromigration is a physical effect of wafer chip scale packages in general, being a first order function of DC current and temperature.

Refer to the application note [TPS62366x Thermal and Device Lifetime Information \(SLVA525\)](#) for detailed information.

For more details on how to use the thermal parameters, see the application notes: [Thermal Characteristics Application Note \(SZZA017\)](#), and [IC Package Thermal Metrics Application Note \(SPRA953\)](#).

## PCB LAYOUT

The PCB layout is an important step to maintain the high performance of the TPS62366x. Both the high current and the fast switching nodes demand full attention to the PCB layout to save the robustness of the TPS62366x through the PCB layout. Improper layout might show the symptoms of poor line or load regulation, ground and output voltage shifts, stability issues, unsatisfying EMI behavior or worsened efficiency.

### Signal Routing Strategy

The TPS62366x is a mixed signal IC. Depending on the function of a pin or trace, different board layout strategies must be addressed to achieve a good design. Due to the nature of a switching converter, some signals are sensitive to influence from other signals (aggressors). The sense lines, SENSE+ and SENSE-, are sensitive to the aggressors, which are high bandwidth I/O pins (SCL and SDA) and the switch node (SW) and their connected traces. Special care must be taken to avoid cross-talk between them.

The following recommendations need to be followed:

- PGND, VIN and SW should be routed on thick layers. They must not surround inner signal layers which are not able to withstand interference from noisy PGND, VIN and SW. They create a flux which is determined by the switching frequency. The flux generated affects neighboring layers due to capacitive coupling across layers.
- AGND, AVIN and VDD must be isolated from noisy signals.
- If crossing layers is required for PGND, VIN and SW, they must be dimensioned to support the high currents to not cause high IR drops. In general, changing the layers frequently must be avoided.
- Signal traces, and especially the sense lines (SENSE+ and SENSE-), must be kept away from noisy traces/signals. Avoid capacitive coupling with neighboring noisy layers by cutting away the overlapping areas close to signal traces. Special care must be taken for the sense lines to avoid inductive / capacitive cross-talk from aggressors, both from noisy lines as well as the external inductor which generates a magnetic field.
- Care should be taken for a proper thermal layout. Wide traces, connecting with vias through the layers, provides a proper thermal path to sink the heat energy created from the device and inductor.

## External Components Placement

The input capacitor at VIN must be placed closest to the IC for proper operation. The decoupling caps at AVIN and VDD reduce noise impacts and should be placed as close to the IC as possible. The output filter, consisting of  $C_{OUT}$  and L, converts the switching signal at SW to the noiseless output voltage. It should be placed as close as possible to the device keeping the switch node small, for best EMI behavior.

## Trace routing

Route the VIN trace wide and thick to avoid IR drops. The trace between the input capacitor's higher node and VIN as well as the trace between the input capacitor's lower node and PGND must be kept as short as possible. Parasitic inductance on these traces must be kept as tiny as possible for proper device operation.

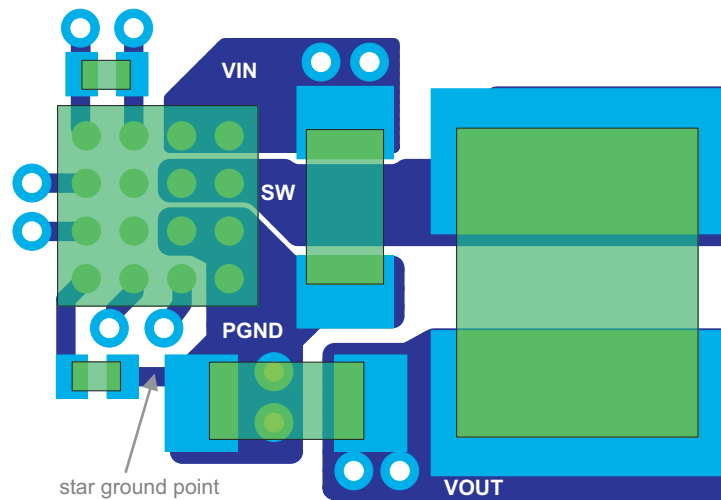
AVIN and AGND should be isolated from noisy signals. Route AGND to the star ground point where no IR drop occurs. The input cap at AVIN isolates noise. Proceed with VDD and AGND in a similar manner.

The switch node trace, SW, must connect directly to the inductor followed by the output capacitors,  $C_{OUT}$ . The switch node is an aggressor. Keeping this trace short reduces noise being radiated and improves EMI behavior. The lower node of the output capacitor,  $C_{OUT}$ , needs to connect to the star ground point. The TPS62366x supports the point of load concept (POL). Input caps at the POL do not need to be placed closest to the IC; they should be placed close to the POL. Route the traces between the TPS62366x's output capacitor and the load's input capacitors direct and wide to avoid losses due to the IR drop.

Connect the sense lines to the POL. This puts into practice the remote sensing concept, allowing the device to regulate the voltage at the POL, compensating IR drops. If possible, make a Kelvin connection to the load device. The sense lines are susceptible to noise. They must be kept away from noisy signals such as PGND, VIN, and SW, as well as high bandwidth signals such as the I<sup>2</sup>C. Avoid both capacitive as well as inductive coupling by keeping the sense lines short, direct and close to each other. Run the lines in a quiet layer. Isolate them from noisy signals by a voltage or ground plane if possible. Running the signal as a differential pair is recommended.

The PGND nodes at  $C_{IN}$  and  $C_{OUT}$  can be connected underneath the IC at the PGND pins (star point). Make sure that small signal traces returning to the AGND do not share the high current path at PGND to  $C_{IN}$  and  $C_{OUT}$ .

See [Figure 53](#) for the recommended layout.



**Figure 53. Layout Suggestion (top view) with 3225 inductor. Overall Solution Size: 27.5mm<sup>2</sup>**

## REGISTER SETTINGS

### Overview

**Table 9. TPS62366A Register Settings Overview**

ADDRESS	REGISTER	RESET / DEFAULT STATE	READ / WRITE	REGISTER (default / reset values)							
				MSB				LSB			
				D7	D6	D5	D4	D3	D2	D1	D0
0x00h	SET0	0100 0110	R/W	MODE0	OV0[6:0]						
0x01h	SET1	0100 0010	R/W	MODE1	OV1[6:0]						
0x02h	(Reserved)	xxxx xxxx	-								
0x03h	(Reserved)	xxxx xxxx	-								
0x04h	Ctrl	11xx xxxx	R/W	PD_EN	PD_VSEL						
0x05h	Temp	xxxx x000	R/W					DIS_TS	TJEW	TJTS	
0x06h	RmpCtrl	000x x00x	R/W	RMP[2:0]				EN_DISC	RAMP_PFM		
0x07h	(Reserved)	xxxx xxxx	-								
0x08h	Chip_ID	1001 00xx	R								
0x09h	Chip_ID										

**Table 10. TPS62366B Register Settings Overview**

ADDRESS	REGISTER	RESET / DEFAULT STATE	READ / WRITE	REGISTER (default / reset values)							
				MSB				LSB			
				D7	D6	D5	D4	D3	D2	D1	D0
0x00h	SET0	0010 1110	R/W	MODE0	OV0[6:0]						
0x01h	SET1	0101 1010	R/W	MODE1	OV1[6:0]						
0x02h	(Reserved)	xxxx xxxx	-								
0x03h	(Reserved)	xxxx xxxx	-								
0x04h	Ctrl	11xx xxxx	R/W	PD_EN	PD_VSEL						
0x05h	Temp	xxxx x000	R/W					DIS_TS	TJEW	TJTS	
0x06h	RmpCtrl	000x x00x	R/W	RMP[2:0]				EN_DISC	RAMP_PFM		
0x07h	(Reserved)	xxxx xxxx	-								
0x08h	Chip_ID	1001 01xx	R								
0x09h	Chip_ID										

**Register 0x00h Description: SET0**

The register settings apply by choosing SET0 (VSEL = LOW).

**Table 11. TPS62366A Register 0x00h Description**

REGISTER ADDRESS: 0x00h Read/Write				
BIT	NAME	DEFAULT	DESCRIPTION	
D7	MODE0	MSB	0 Operation mode for SET0 0 = PFM / PWM mode operation 1 = Forced PWM mode operation	
D6	OV0[6:0]	1	Output voltage for SET0 Default: (100 0110) <sub>2</sub> = 1.2V	
D5		0		
D4		0		D6-D0      Output voltage
D3		0		000 0000    500 mV
D2		1		000 0001    510 mV
				000 0010    520 mV
D1		1		...            ... 111 1111    1770 mV
D0	LSB	0	$V_{OUT} = (xxx\ xxx)_2 \times 10mV + 500\ mV$	

**Table 12. TPS62366B Register 0x00h Description**

REGISTER ADDRESS: 0x00h Read/Write				
BIT	NAME	DEFAULT	DESCRIPTION	
D7	MODE0	MSB	0 Operation mode for SET0 0 = PFM / PWM mode operation 1 = Forced PWM mode operation	
D6	OV0[6:0]	0	Output voltage for SET0 Default: (010 1110) <sub>2</sub> = 0.96V	
D5		1		
D4		0		D6-D0      Output voltage
D3		1		000 0000    500 mV
D2		1		000 0001    510 mV
				000 0010    520 mV
D1		1		...            ... 111 1111    1770 mV
D0	LSB	0	$V_{OUT} = (xxx\ xxx)_2 \times 10mV + 500\ mV$	

**Register 0x01h Description: SET1**

The register settings apply by choosing SET1 (VSEL = HIGH).

**Table 13. TPS62366A Register 0x01h Description**

REGISTER ADDRESS: 0x01h Read/Write					
BIT	NAME	DEFAULT	DESCRIPTION		
D7	MODE1	MSB	0 Operation mode for SET1 0 = PFM / PWM mode operation 1 = Forced PWM mode operation		
D6	OV1[6:0]	1	Output voltage for SET1 Default: $(100\ 0010)_2 = 1.16\text{V}$		
D5		0			
D4		0		D6-D0	Output voltage
D3		0		000 0000	500 mV
D2		0		000 0001	510 mV
				000 0010	520 mV
D1		1		...	...
				111 1111	1770 mV
D0	LSB	0	$V_{OUT} = (xxx\ xxxx)_2 \times 10\text{mV} + 500\ \text{mV}$		

**Table 14. TPS62366B Register 0x01h Description**

REGISTER ADDRESS: 0x01h Read/Write					
BIT	NAME	DEFAULT	DESCRIPTION		
D7	MODE1	MSB	0 Operation mode for SET1 0 = PFM / PWM mode operation 1 = Forced PWM mode operation		
D6	OV1[6:0]	1	Output voltage for SET1 Default: $(101\ 1010)_2 = 1.40\text{V}$		
D5		0			
D4		1		D6-D0	Output voltage
D3		1		000 0000	500 mV
D2		0		000 0001	510 mV
				000 0010	520 mV
D1		1		...	...
				111 1111	1770 mV
D0	LSB	0	$V_{OUT} = (xxx\ xxxx)_2 \times 10\text{mV} + 500\ \text{mV}$		

**Register 0x04h Description: Ctrl**

**Table 15. TPS62366x Register 0x04h Description**

REGISTER ADDRESS: 0x04h Read / Write			
BIT	NAME	DEFAULT	DESCRIPTION
D7	PD_EN	MSB	1 EN internal pull down resistor 0 = disabled 1 = enabled
D6	PD_VSEL		1 VSEL internal pull down resistor 0 = disabled 1 = enabled
D5			x Reserved for future use
D4			x Reserved for future use
D3			x Reserved for future use
D2			x Reserved for future use
D1			x Reserved for future use
D0			LSB x Reserved for future use

**Register 0x05h Description: Temp**

**Table 16. TPS62366x Register 0x05h Description**

REGISTER ADDRESS: 0x05h Read/Write			
BIT	NAME	DEFAULT	DESCRIPTION
D7		MSB	x Reserved for future use
D6			x Reserved for future use
D5			x Reserved for future use
D4			x Reserved for future use
D3			x Reserved for future use
D2	DIS_TS	0	Disable temperature shutdown feature 0 = Temperature shutdown enabled 1 = Temperature shutdown disabled (not recommended)
D1	TJEW	0	T <sub>J</sub> early warning bit 0 = T <sub>J</sub> < 120°C (typ) 1 = T <sub>J</sub> ≥ 120°C (typ)
D0	TJTS	0	T <sub>J</sub> temperature shutdown bit 0 = die temperature within the valid range 1 = temperature shutdown was triggered Bit needs to be reset after it has been latched.
		LSB	

**Register 0x06h Description: RmpCtrl**
**Table 17. TPS62366x Register 0x06h Description**

REGISTER ADDRESS: 0x06h Read/Write					
BIT	NAME	DEFAULT	DESCRIPTION		
D7	RMP[2:0]	MSB	Output voltage ramp timing		
D6			0	D7-D5	Slope
				000	32 mV / $\mu$ s
				001	16 mV / $\mu$ s
				010	8 mV / $\mu$ s
				...	...
				110	0.5 mV / $\mu$ s
				111	0.25 mV / $\mu$ s
D5			0	$\frac{\Delta V_{OUT}}{\Delta t} = 32 \frac{mV}{\mu s} \frac{1}{2^{(RMP[2-0])_2}}$	
D4			x	Reserved for future use	
D3	x	Reserved for future use			
D2	EN_DISC	0	Active output capacitor discharge at shutdown 0 = disabled 1 = enabled		
D1	RAMP_PFM	0	Defines the ramp behavior if the device is in Power Save (PFM) mode 0 = output cap is discharged by the load only 1 = output voltage is forced to follow the ramp down slope		
D0		LSB	x Reserved for future use		

**Register 0x07h Description: (Reserved)**
**Table 18. TPS62366x Register 0x07h Description**

REGISTER ADDRESS: 0x07h			
BIT	NAME	DEFAULT	DESCRIPTION
D7		MSB	x Reserved for future use
D6			x Reserved for future use
D5			x Reserved for future use
D4			x Reserved for future use
D3			x Reserved for future use
D2			x Reserved for future use
D1			x Reserved for future use
D0			LSB

Register 0x08h, 0x09h Description Chip\_ID:

Table 19. TPS62366x Register 0x08h and 0x09h Description

REGISTER ADDRESS: 0x08h, 0x09 Read				
BIT	NAME	DEFAULT	DESCRIPTION	
D7		MSB	Vendor ID	
D6				1
D5				0
D4				0
D3		x	D3-D2	Part number ID
D2			00	TPS62366A
			01	TPS62366B
			10	-
D1		x	D1-D0	Chip revision ID
D0			00	Rev. 1
			01	Rev. 2
			10	Rev. 3
		LSB	11	Rev. 4

## PACKAGE SUMMARY

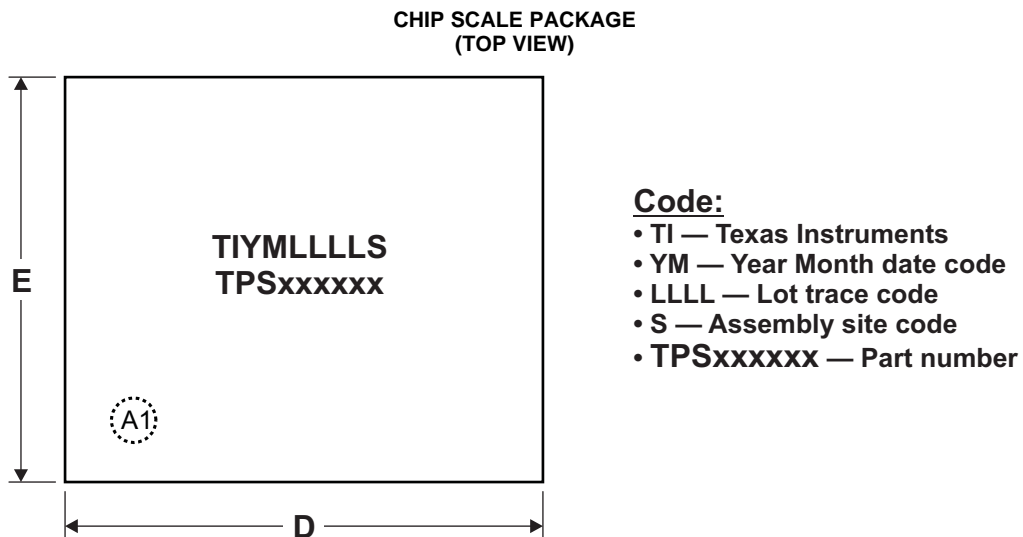


Figure 54. Package Marking and Dimensions

### CHIP SCALE PACKAGE DIMENSIONS

The TPS62366x device is available in a 16-bump chip scale package (YZH, NanoFree™). The package dimensions are given as:

- D = 2.076mm (+/- 0.03mm)
- E = 2.076mm (+/- 0.03mm)

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TPS62366AYZHR	ACTIVE	DSBGA	YZH	16	3000	RoHS & Green	SNAGCU	Level-1-260C-UNLIM	-40 to 85	TPS62366A	<a href="#">Samples</a>
TPS62366AYZHT	ACTIVE	DSBGA	YZH	16	250	RoHS & Green	SNAGCU	Level-1-260C-UNLIM	-40 to 85	TPS62366A	<a href="#">Samples</a>
TPS62366BYZHR	ACTIVE	DSBGA	YZH	16	3000	RoHS & Green	SNAGCU	Level-1-260C-UNLIM	-40 to 85	TPS62366B	<a href="#">Samples</a>
TPS62366BYZHT	ACTIVE	DSBGA	YZH	16	250	RoHS & Green	SNAGCU	Level-1-260C-UNLIM	-40 to 85	TPS62366B	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSELETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "-" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

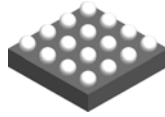
(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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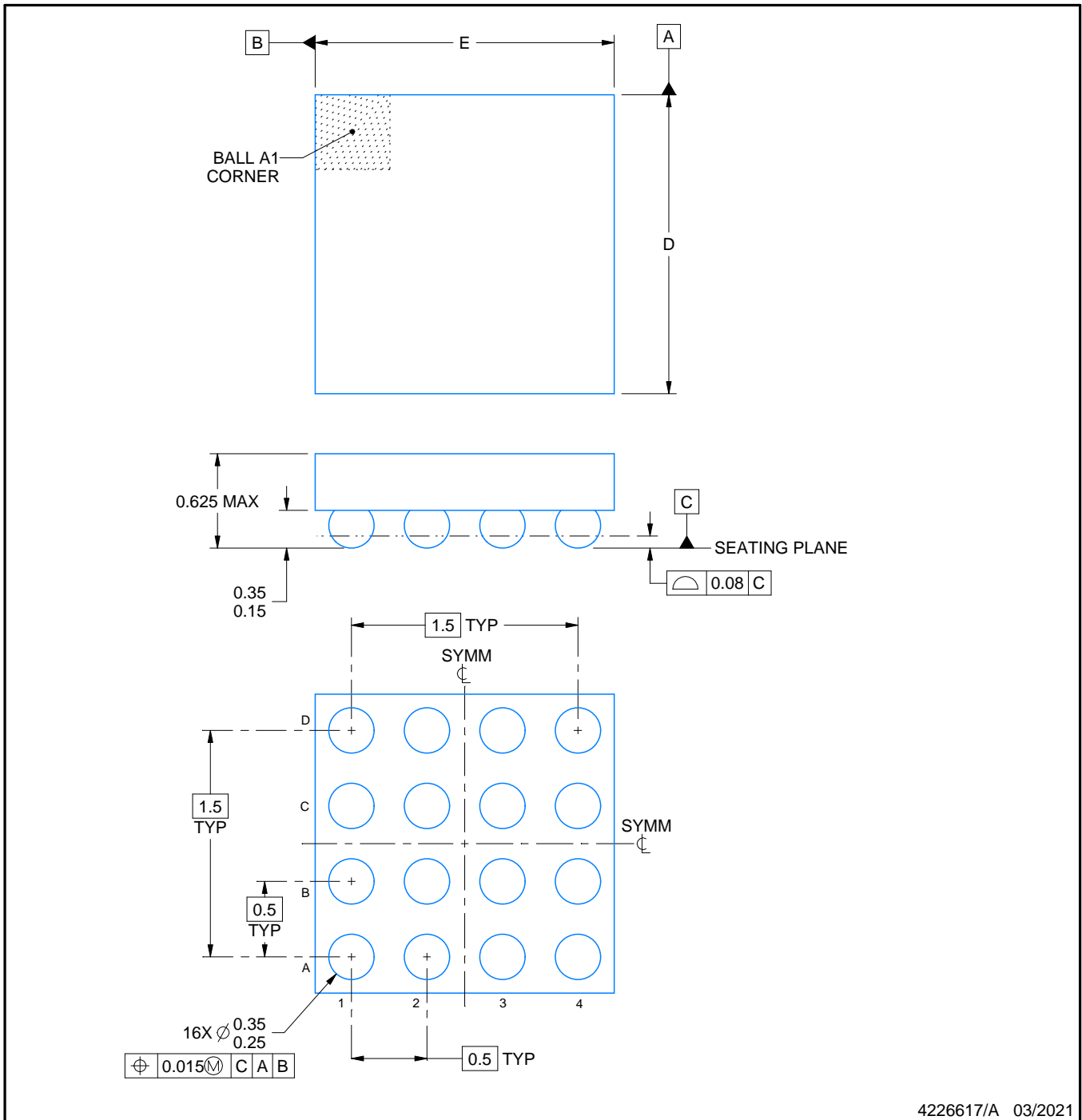
YZH0016



PACKAGE OUTLINE

DSBGA - 0.625 mm max height

DIE SIZE BALL GRID ARRAY



NOTES:

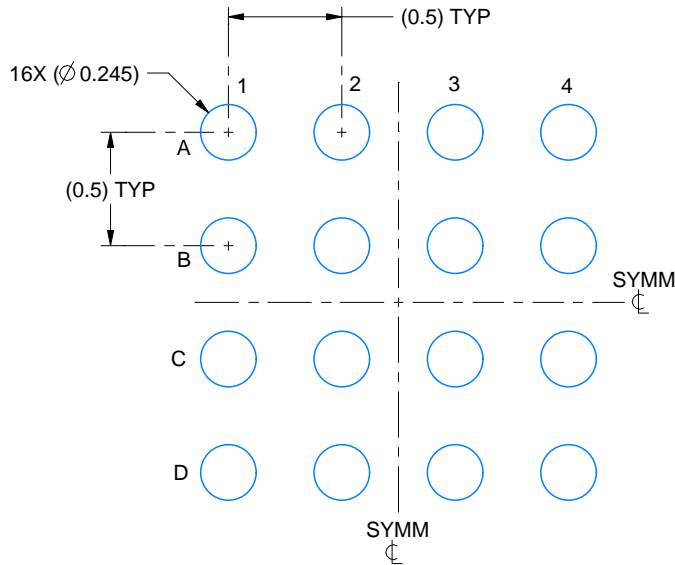
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.

# EXAMPLE BOARD LAYOUT

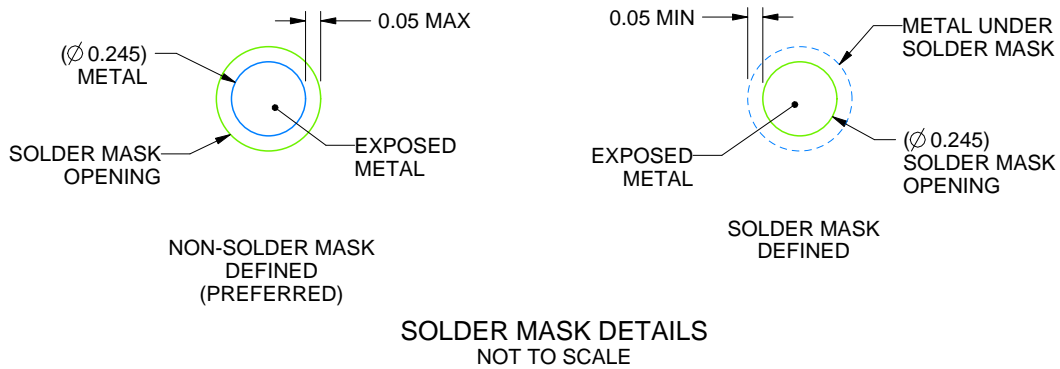
YZH0016

DSBGA - 0.625 mm max height

DIE SIZE BALL GRID ARRAY



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE: 30X



SOLDER MASK DETAILS  
NOT TO SCALE

4226617/A 03/2021

NOTES: (continued)

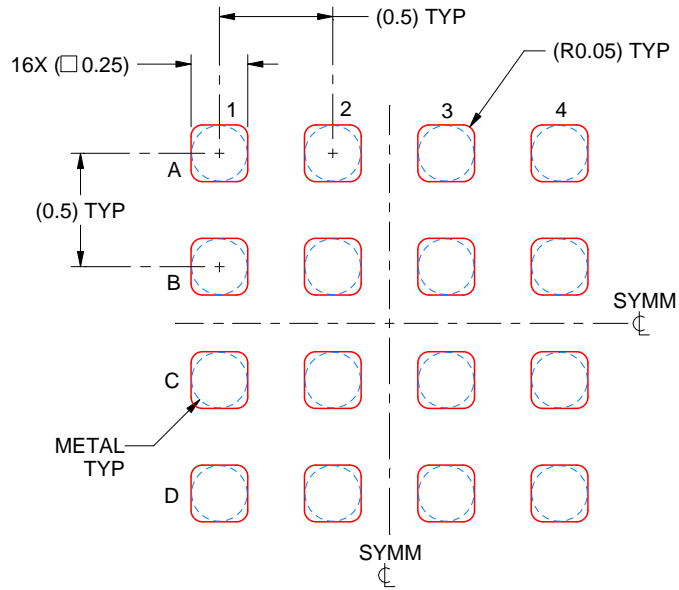
- Final dimensions may vary due to manufacturing tolerance considerations and also routing constraints. See Texas Instruments Literature No. SNVA009 ([www.ti.com/lit/snva009](http://www.ti.com/lit/snva009)).

# EXAMPLE STENCIL DESIGN

YZH0016

DSBGA - 0.625 mm max height

DIE SIZE BALL GRID ARRAY



SOLDER PASTE EXAMPLE  
BASED ON 0.075 mm THICK STENCIL  
SCALE: 30X

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NOTES: (continued)

4. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release.

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